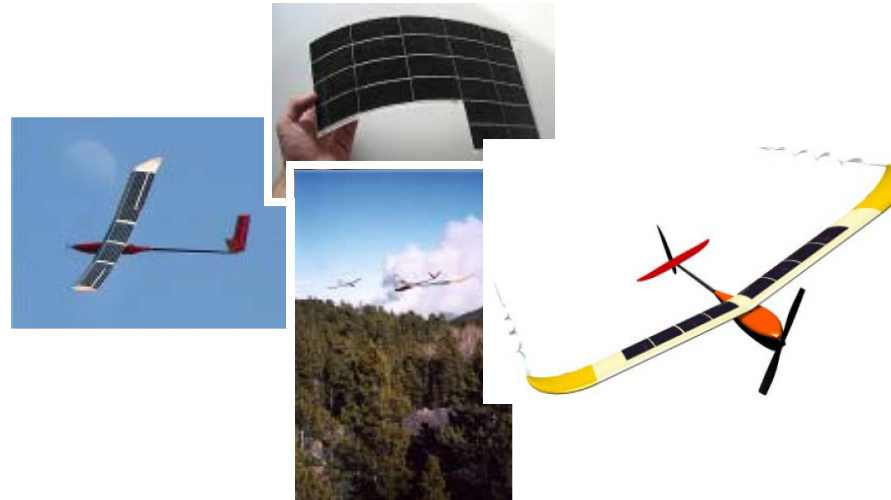




Design of Solar Powered Airplanes for Continuous Flight



André Noth

Doctoral Exam – September 30, 2008

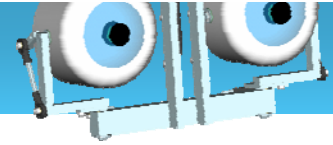
ETH

Eidgenössische Technische Hochschule Zürich
Swiss Federal Institute of Technology Zurich

<http://www.sky-sailor.ethz.ch/>
E-mail: andre.noth@a3.epfl.ch



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- Introduction
- Design Methodology
- Sky-Sailor Design
- Sky-Sailor Prototype
- Scaling
- Conclusion



Motivations & Objective



- Project started with an ESA feasibility study

Introduction

- Motivations
- History of Solar Flight
- State of the Art
- Contributions

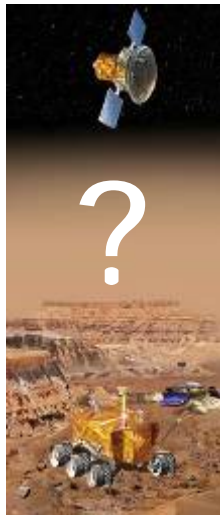
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Mars exploration

Satellites + extensive coverage, good resolution
- place of interest not freely selectable

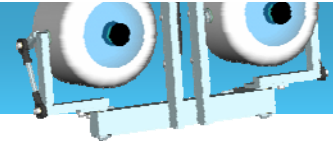
Gap for systems with + high-resolution imagery
+ extensive & selectable coverage

Rovers + excellent resolution, ground interaction
- reduced range, limited by terrain

- ➔ Study the feasibility of solar powered flight on Mars
- ➔ Develop and realize a fully functional prototype on Earth and demonstrate continuous flight



History of Solar Flight



- Started in 1974
- 90 solar powered airplanes listed from 1974 to 2008

Introduction

- Motivations
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Sunrise (1974)
1st solar powered flight



Gossamer Penguin (1980)
1st manned solar powered flight



Sunseeker (1990)
manned, crossed the USA in 21 flight



Solong (2005)
1st continuous flight, used thermals



Solar Riser (1979)
manned, battery solar charged for short flights



Solar Challenger (1981)
manned, channel crossing



Helios (1999)
unmanned, flew at > 29'000 m



Zephyr (2005)
unmanned, flew 83h



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State of the art



Many solar airplanes in History

→ ... but no clear design methodologies explained

→ anyway useful practical papers on case studies

[BOUCHER79, MACCREADY83, COLELLA94]



[ULM96, BRUSS91]

Many design methodologies...

→ ... but rarely validated with a prototype [REHMET97, WEIDER06]

→ very often nice design methods

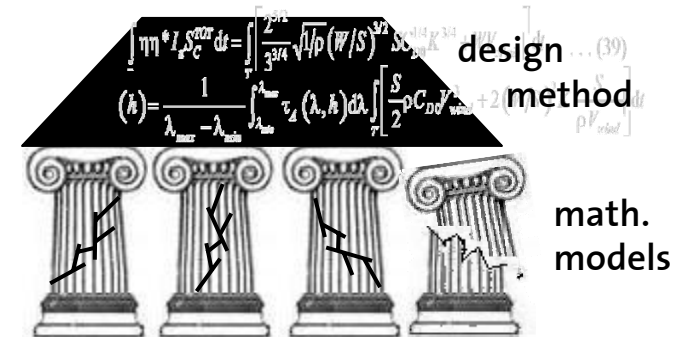
[IRVING74, YOUNGBLOOD82, BAILEY92]

but based on weak models for:

- Weight prediction
- Efficiencies

→ ends with unrealistic designs

[RIZZO08, ROMEO04]



Introduction

- Motivations
- History of Solar Flight
- State of the Art
- Contributions

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Introduction

- Motivations
- History of Solar Flight
- State of the Art
- **Contributions**

Design Methodology

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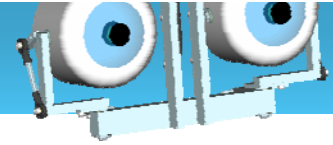
- **Design methodology**
 - Simplicity
 - Large design space
 - Concrete and experienced based
 - Flexible and versatile
- **Theory validation with a prototype**
 - Achieve > 24h flight
 - Autonomous control
- **Draw up a state of the art on solar aviation**
 - History
 - Publications



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Design Methodology



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Design Methodology

- Required Energy
- Solar Energy
- Weight Models
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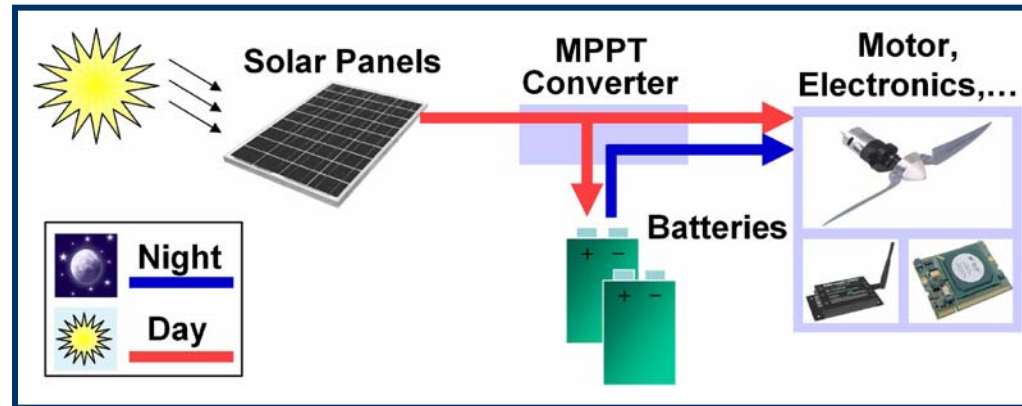
Sky-Sailor Design

Sky-Sailor Prototype

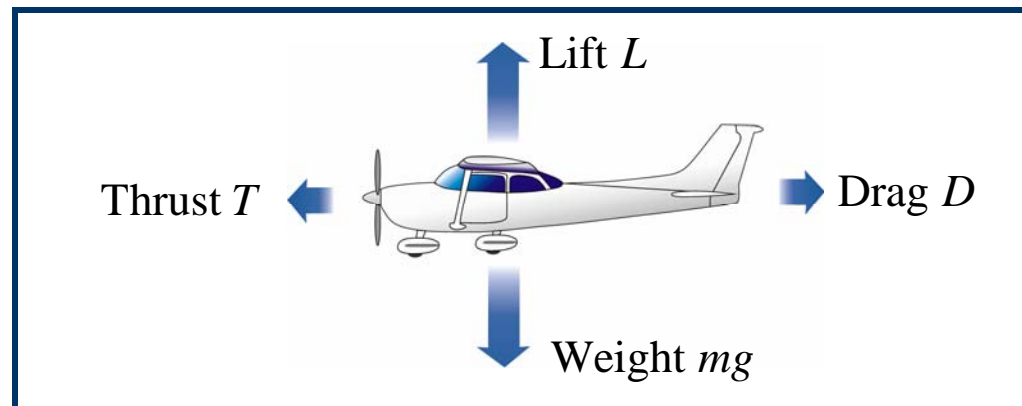
Scaling

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Energy balance



Weight balance



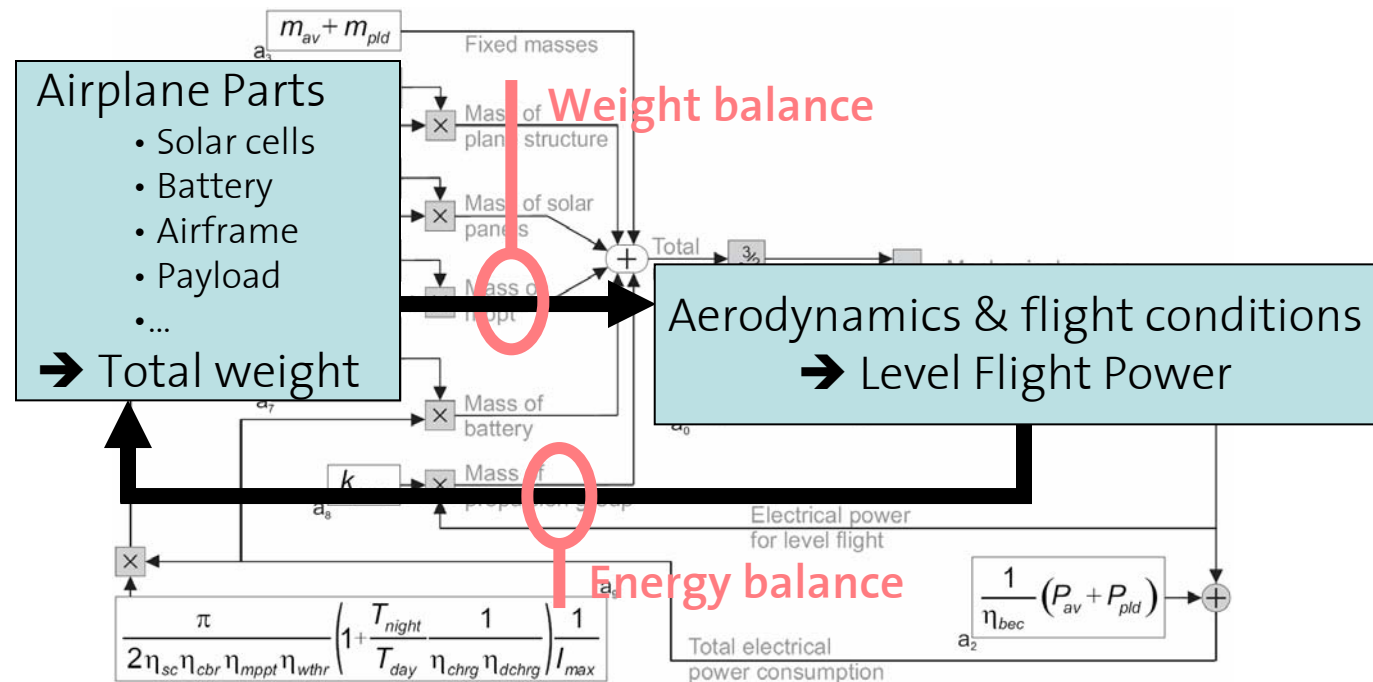
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Methodology



- Sizing the airplane : hen & egg problem



- This loop can be solved:

A Iteratively (trying existing components, refining the design)

B Analytically (using mathematic models of the components)

→ Allows to establish some general design principles

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Required Energy



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Scaling

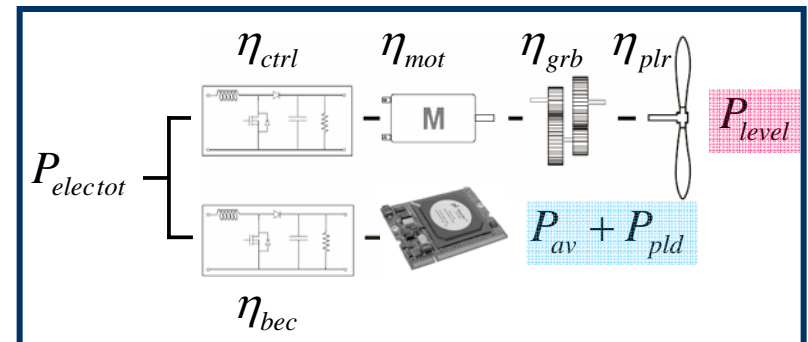
Conclusion

- Equilibrium at steady level flight

$$\left. \begin{aligned} L = mg = C_L \frac{\rho}{2} S v^2 \\ D = T = C_D \frac{\rho}{2} S v^2 \end{aligned} \right\} P_{level} = D v = \frac{C_D}{C_L^{3/2}} \sqrt{\frac{(mg)^3}{S}} \sqrt{\frac{2}{\rho}}$$

- Power required

$$P_{electot} = \frac{1}{\eta_{ctrl} \eta_{mot} \eta_{grb} \eta_{plr}} P_{level} + \frac{1}{\eta_{bec}} (P_{av} + P_{pld})$$



- Daily energy required

$$E_{elec\ tot} = P_{elec\ tot} \left(T_{day} + \frac{T_{night}}{\eta_{chrg} \eta_{dchrg}} \right)$$



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Required Energy



Introduction

Design Methodology

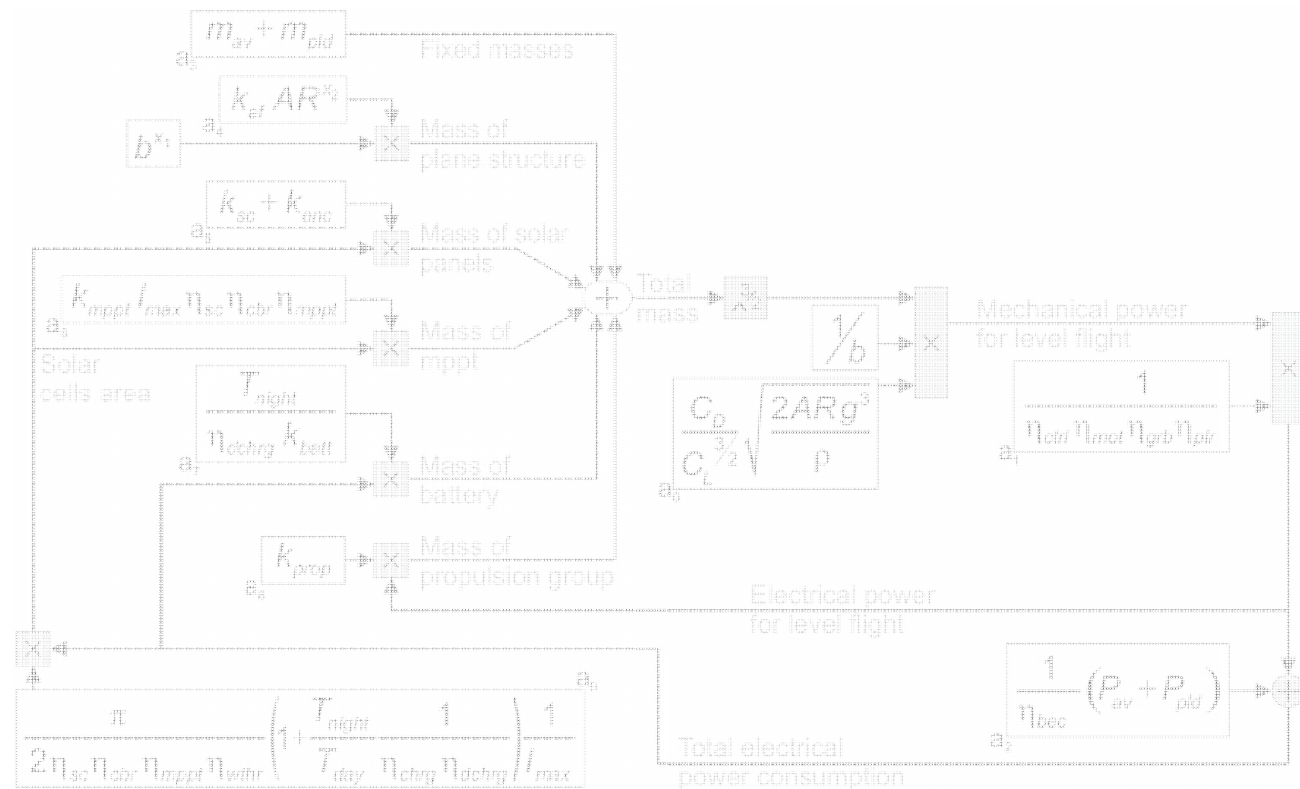
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Solar Energy



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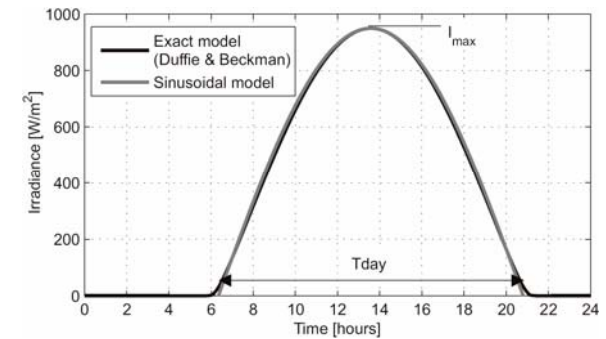
Conclusion

- Daily average solar irradiance

– Irradiance ~ cosine

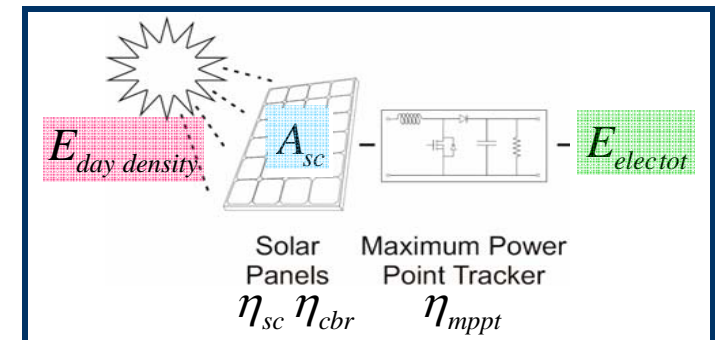
$$E_{\text{day density}} = \frac{I_{\text{max}} T_{\text{day}}}{\pi / 2} \eta_{\text{wthr}}$$

– $I_{\text{max}} T_{\text{day}} = f(\text{date, location, weather})$



- Daily energy obtained

$$E_{\text{elector}} = E_{\text{day density}} A_{\text{sc}} \eta_{\text{sc}} \eta_{\text{cbr}} \eta_{\text{mppt}}$$



- Daily energy required = Daily energy obtained

➔ We compute A_{sc}



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Required Energy



Introduction

Design Methodology

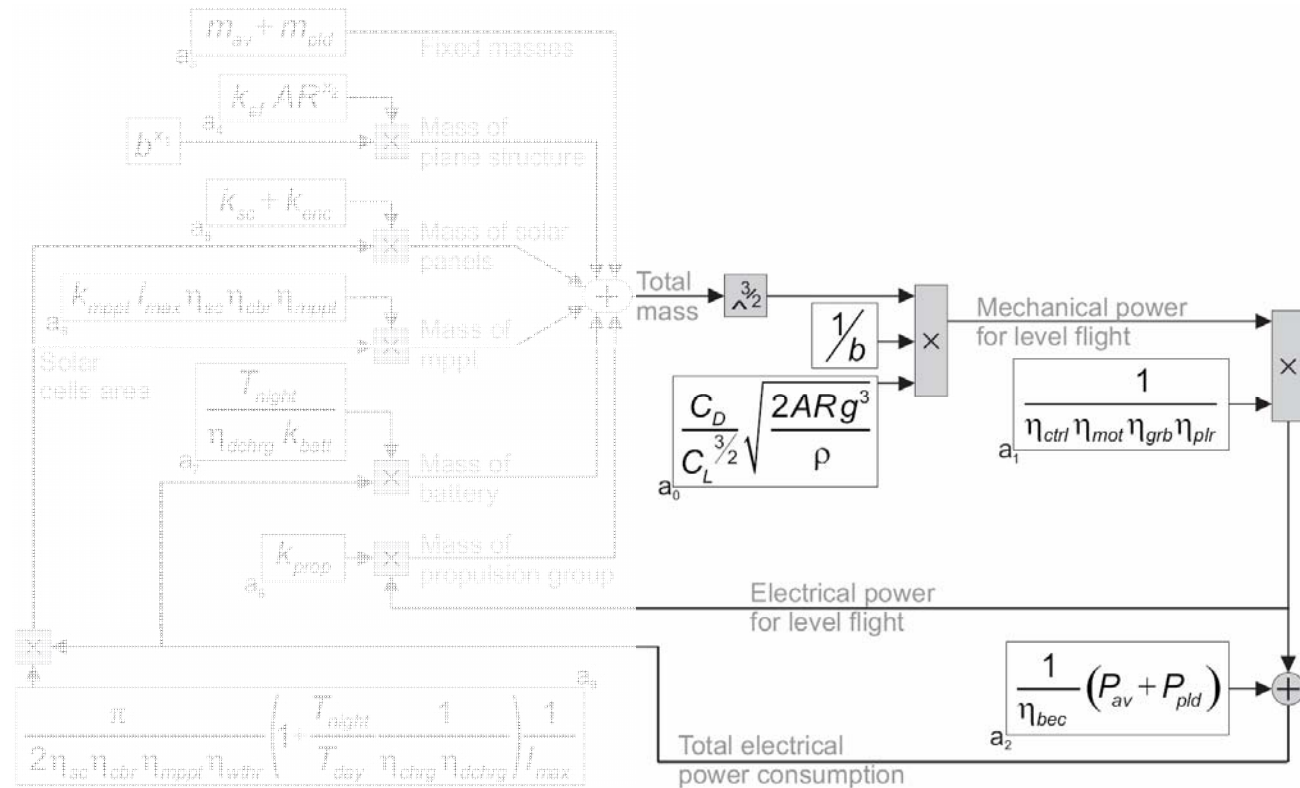
- Required Energy
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Introduction

Design Methodology

- Required Energy
- Solar Energy
- **Weight Models**
- Resolution

Sky-Sailor Design

Sky-Sailor Prototype

Scaling

Conclusion

• Fixed Masses

- Payload m_{pld}
- Avionic System (Autopilot) m_{av}

• Airplane Structure

– In the literature

- [BRANDT95, GUGLIERI96,...] consider $W_{af} = k \cdot S$
 - valid locally
- [HALL68] calculated all airframe elements separately
 - complex, only valid for 1000-3000 lbs airplanes
- [STENDER69] proposed $W_{af} = 8.763 n^{0.311} S^{0.778} AR^{0.467}$
 - very widely adopted
 - adapted by [RIZZO04] to UAV $W_{af} = 15.19 S^{0.656} AR^{0.651}$



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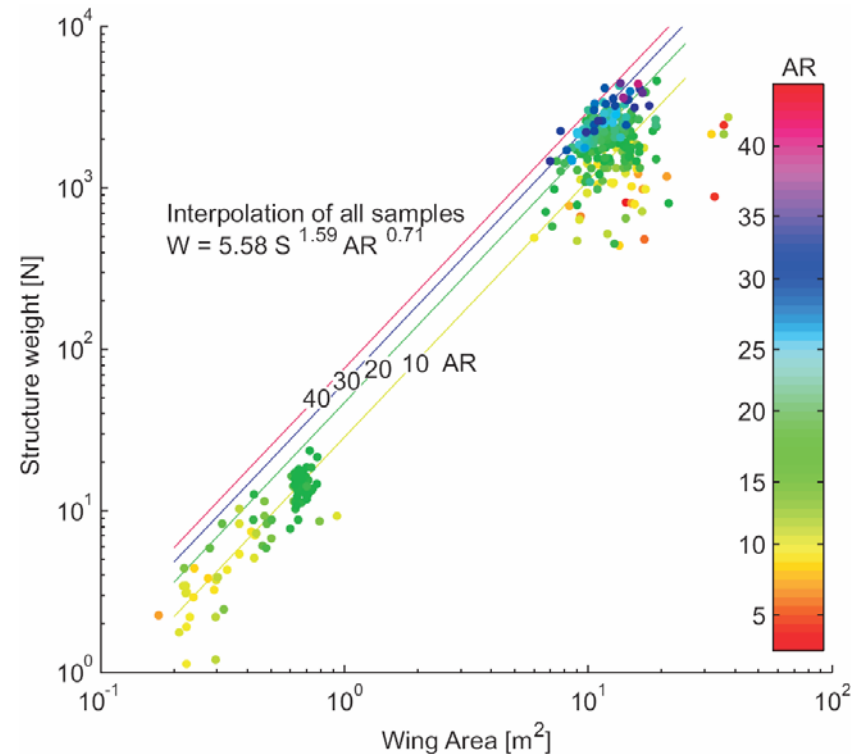
Weight Prediction Models



- Verification of these models
 - Database of 415 sailplane
 - Structure Weight vs Area
 - Models don't fit well

- New model proposed
 - Same equation, new coef.
 - Least square method fit
 - Data set divided in two
 - 5 iterations = 5 qualities
 - Best 5% model:

$$W_{af} = 0.44 b^{3.10} \cdot AR^{-0.25}$$



Introduction

Design Methodology

- Required Energy
- Solar Energy
- Weight Models
- Resolution

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Weight Prediction Models

Biologists already studied flying in nature to extract tendencies

[TENNEKES92] presented the « Great Flight Diagram »
Clear cubic tendency

Our model is // to Tennekes curve

[STENDER69,RIZZO04] seem incoherent

Introduction

Design Methodology

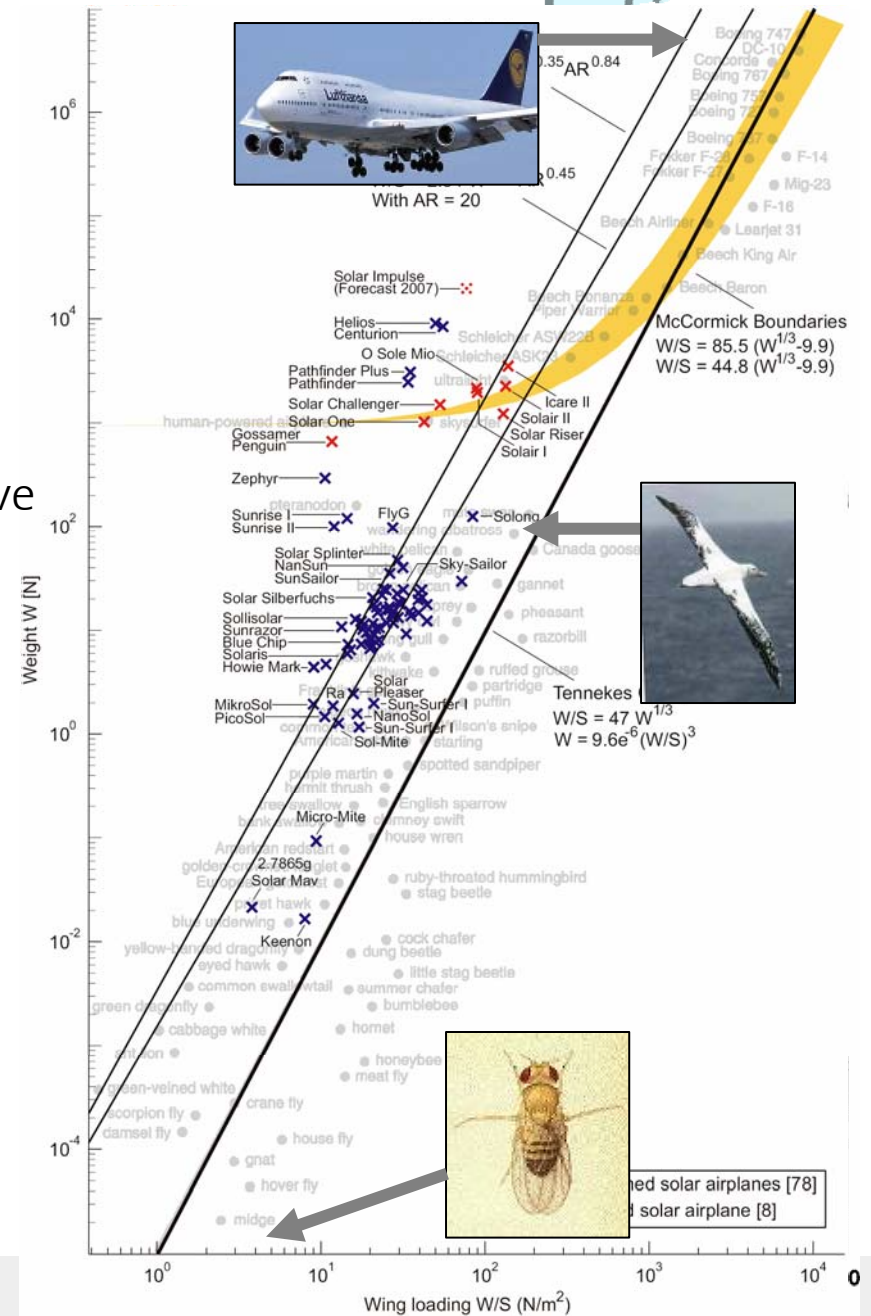
- Required Energy
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Required Energy



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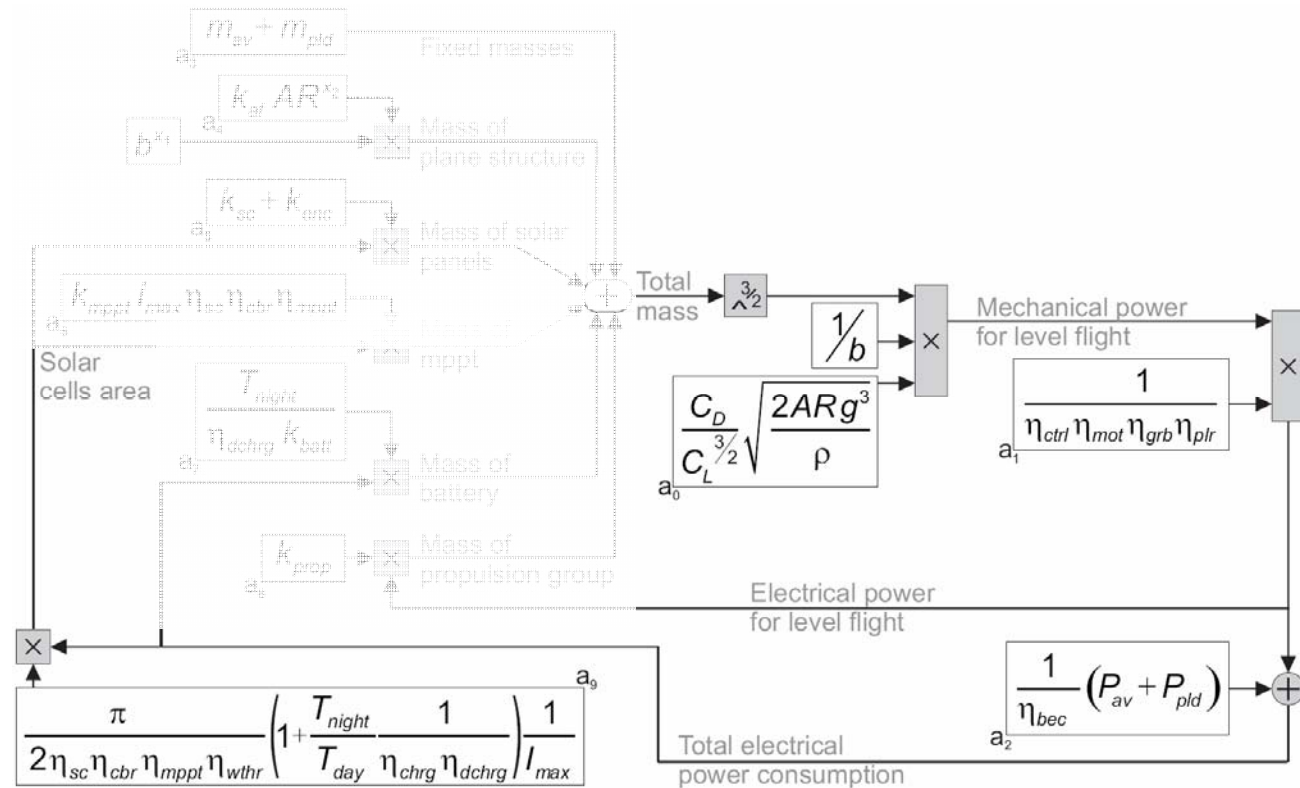
- Required Energy
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Weight Prediction Models



• Solar Cells

- Surface = f(cells properties, required energy)
- Weight proportionnal to the surface

$$m_{sc} = A_{sc} (k_{sc} + k_{enc})$$

• Maximum Power Point Tracker

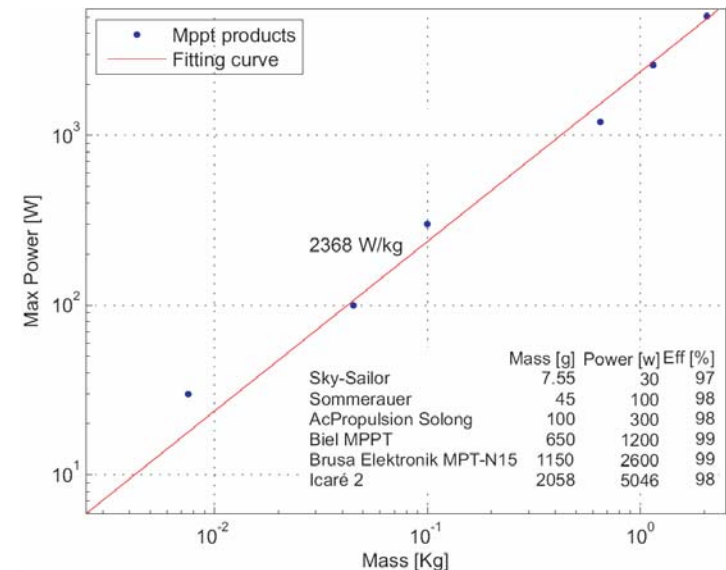
- Study of high efficiency MPPT
- ➔ Weight linear with P_{max}

$$\begin{aligned} m_{mppt} &= k_{mppt} P_{sol\ max} \\ &= k_{mppt} I_{max} \eta_{sc} \eta_{cbr} \eta_{mppt} A_{sc} \end{aligned}$$

• Batterie

- Weight proportionnal to capacity

$$m_{bat} = \frac{T_{night}}{\eta_{dchrg} k_{bat}} P_{elec\ tot}$$



Introduction

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- Required Energy
- Solar Energy
- Weight Models
- Resolution

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Required Energy



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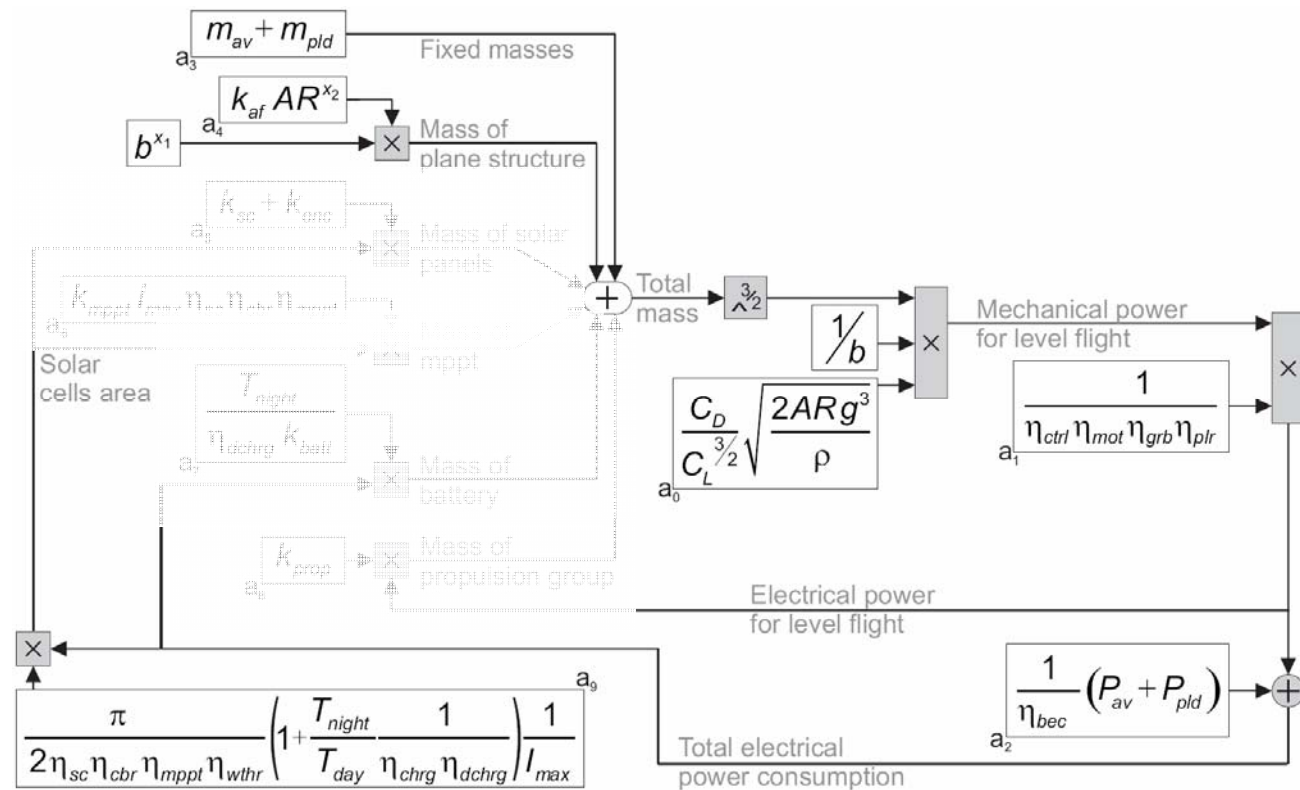
- Required Energy
- Solar Energy
- **Weight Models**
- Resolution

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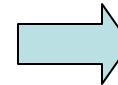
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Weight Prediction Models

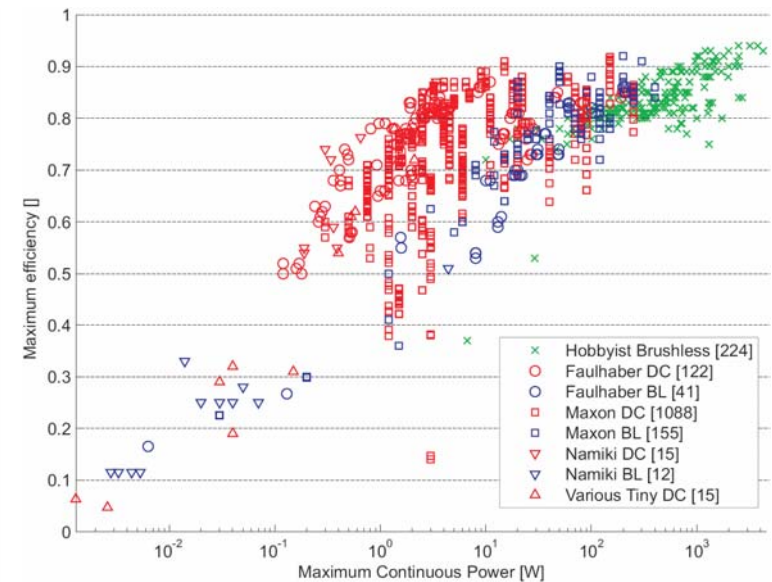
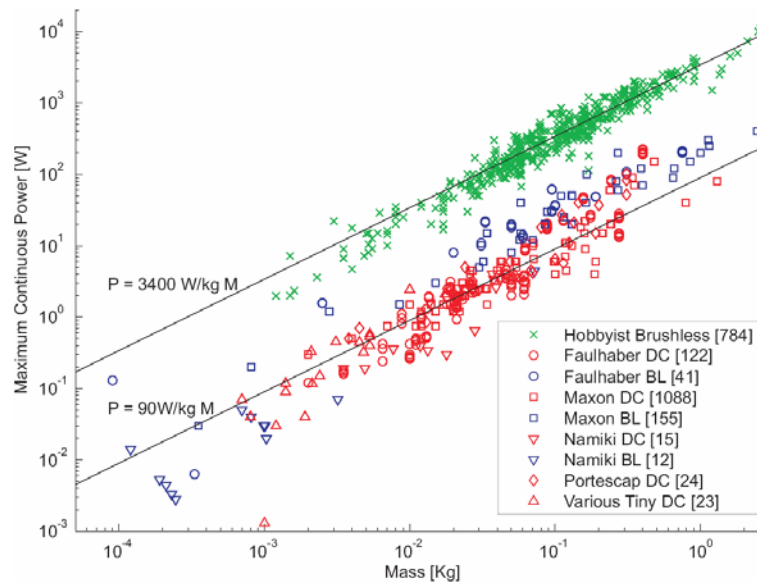


- Propulsion group
 - Existing models but none is proven on a large range
 - Very large databases created

2264 motors
170 electronics controllers
997 gearboxes
673 propellers



Interpolated Models



Introduction

Design Methodology

- Required Energy
- Solar Energy
- Weight Models
- Resolution

Sky-Sailor Design

Sky-Sailor Prototype

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Keywords: Mass to power ratio of motors / Power to mass ratio of electrical motors, piezoelectric motors, Motor mass to power ratio / Motor power to mass ratio of electromagnetic motors, brushed and brushless motors energy density, power density, density of energy, density of power.

Summary and Resolution



Introduction

Design Methodology

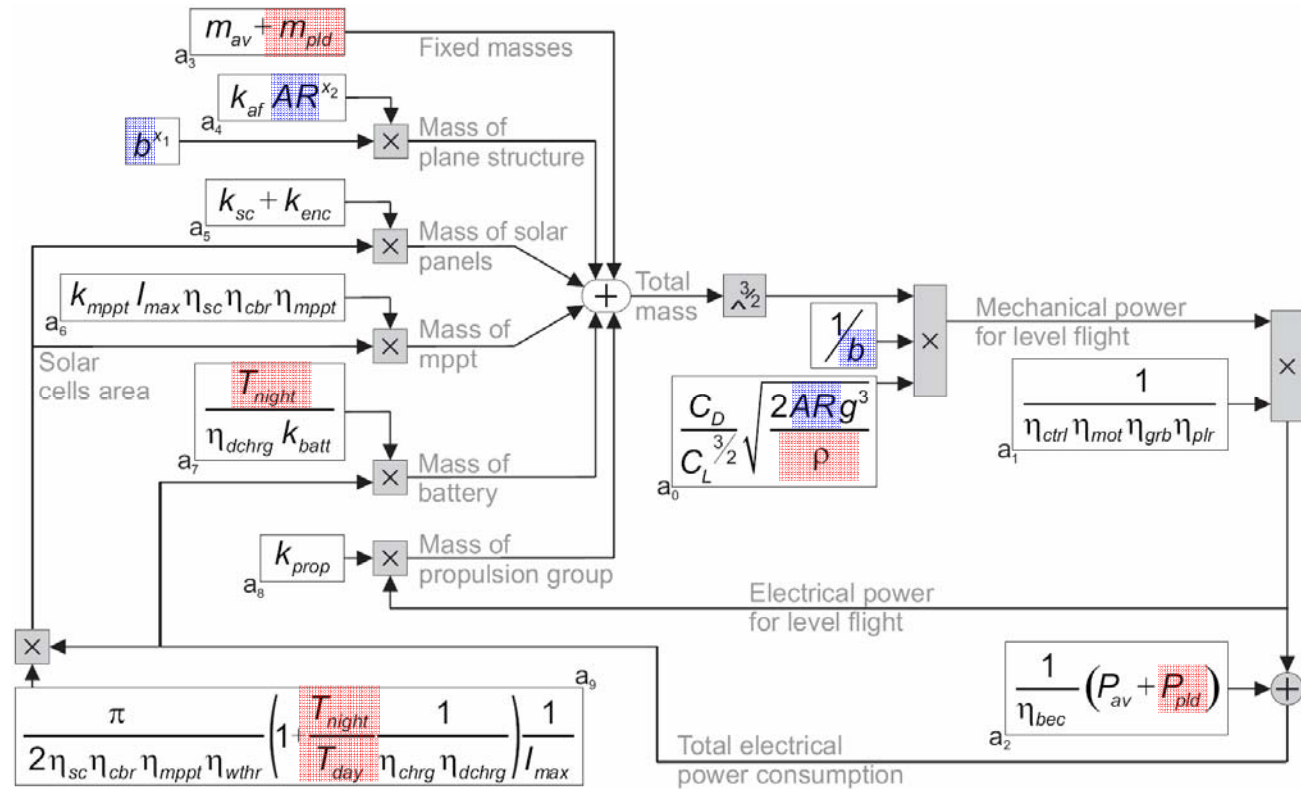
- Required Energy
- Solar Energy
- Weight Models
- Resolution

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Scaling

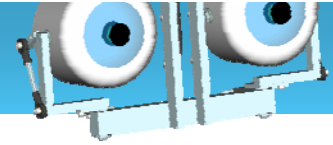
Conclusion



→ Search b and AR for which the loop has a solution



Sky-Sailor Design



Introduction

Design Methodology

Sky-Sailor Design

- Math. Application
- Real-Time Simulation

Sky-Sailor Prototype

Scaling

Conclusion



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Methodology application



- **Mission parameters**

- Solar flight possible 3 months in summer ($T_{\text{day}}=13.2\text{h}$)
- 50g payload consuming 0.5W
- Flight location CH, at 500m above sea level

Introduction

Design Methodology

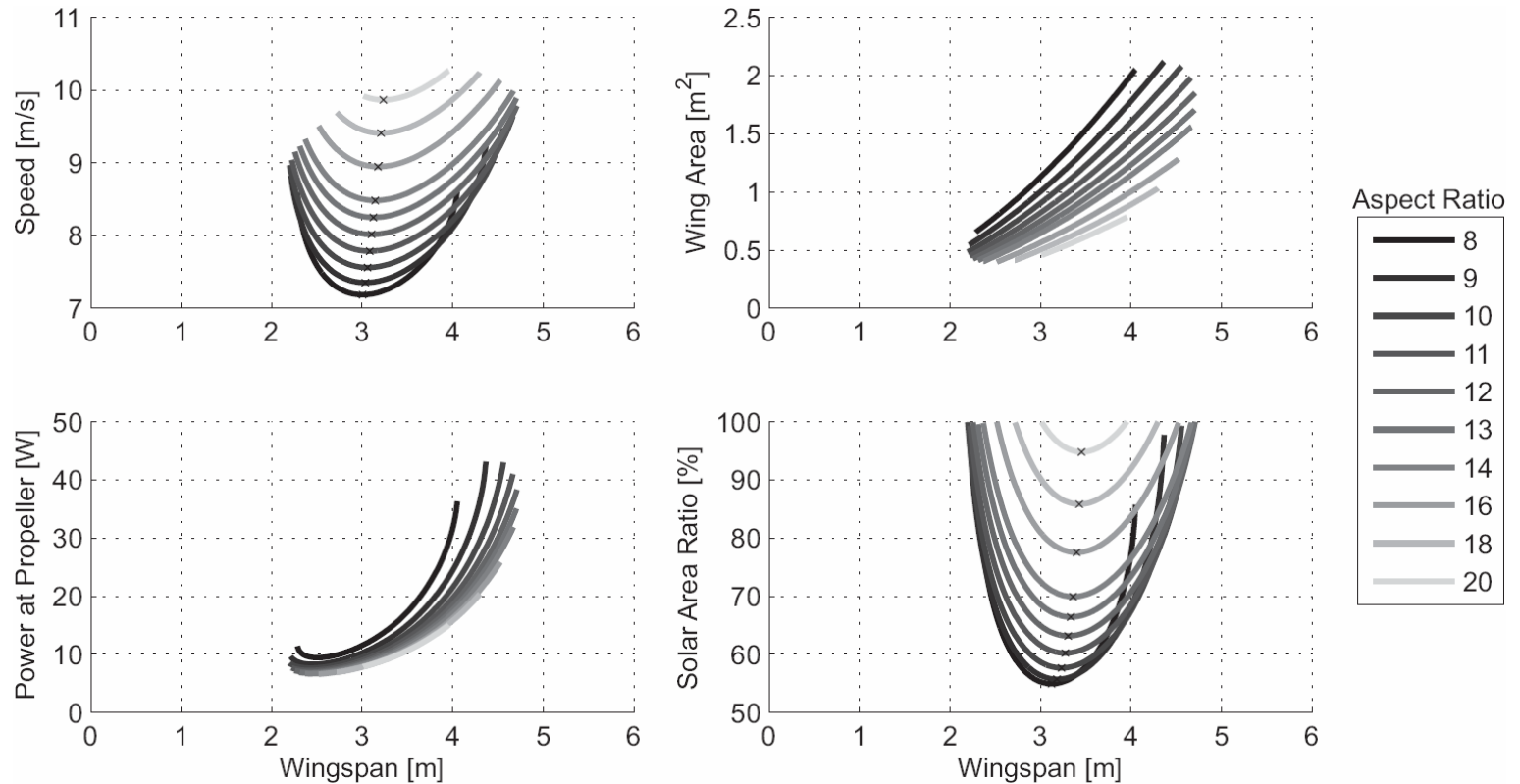
Sky-Sailor Design

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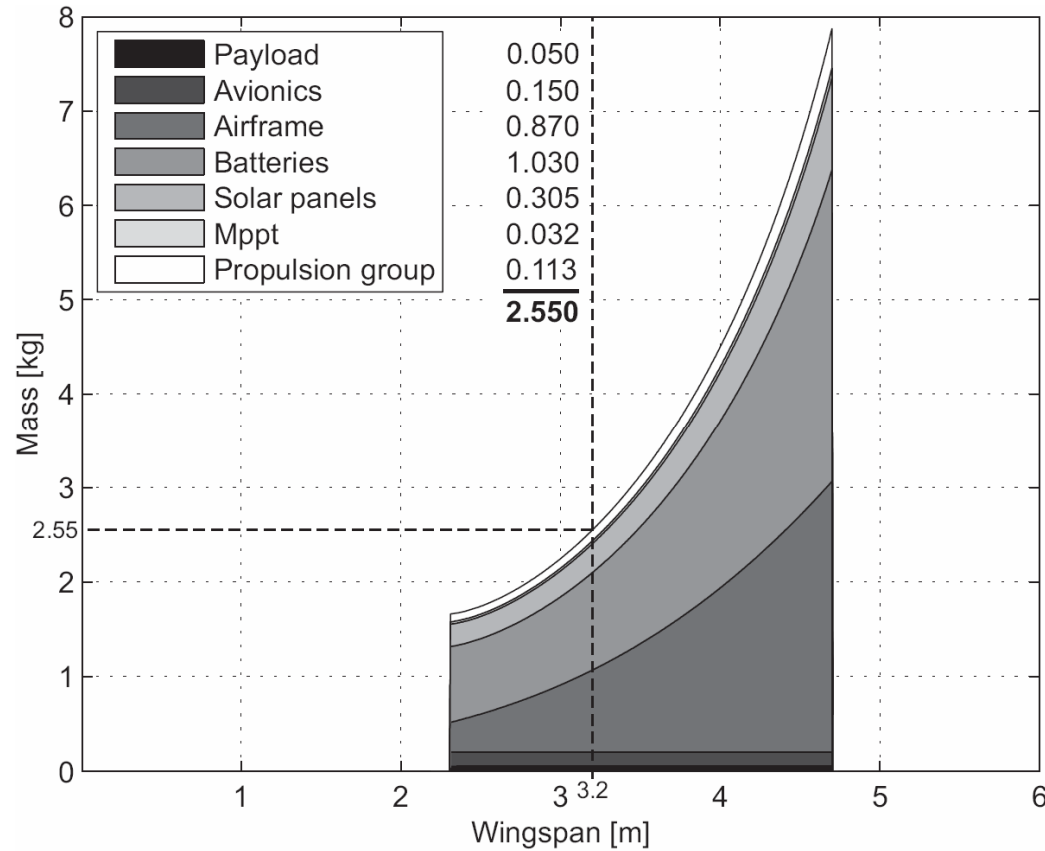
Sky-Sailor Design

- Meth. Application
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• Sky-Sailor Layout

- 3.2m wingspan
- 0.78m² wing area (0.525m² covered by cells)
- 14.2W for level flight (electrical)



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Real-Time Simulation



Objectives

- Validate the design
- Analyze energy flows on the airplane each second
- Rapidly see influence of parameters change

Introduction

Design Methodology

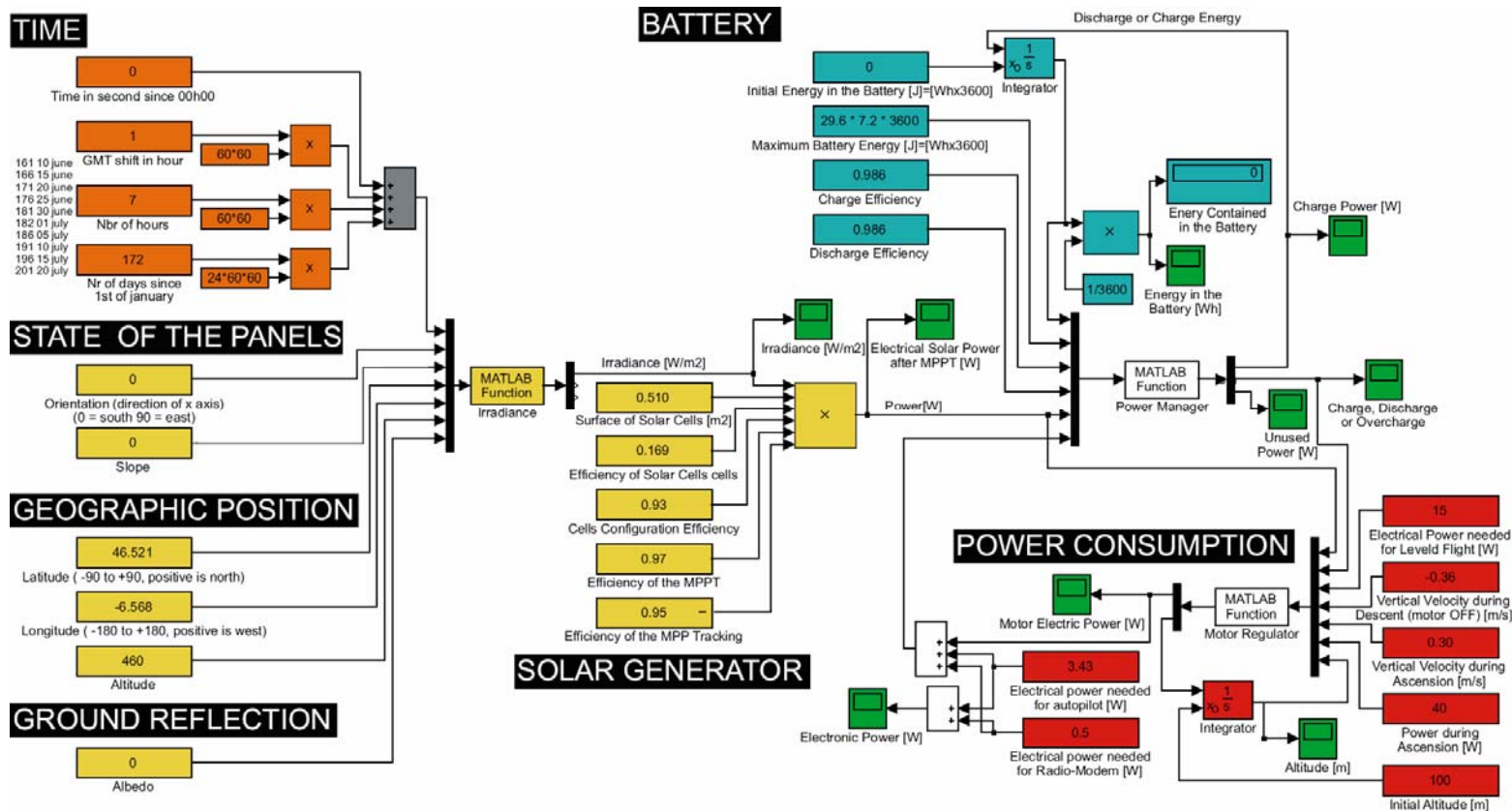
Sky-Sailor Design

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Real-Time Simulation



Simulation of a 48 h flight

- On the 21st of June
- On the 4th of August (+1.5 month)

Introduction

Design Methodology

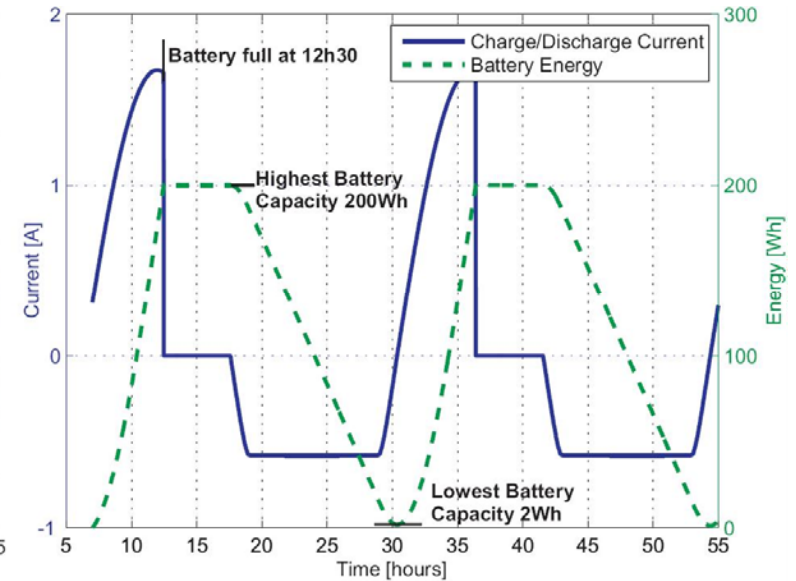
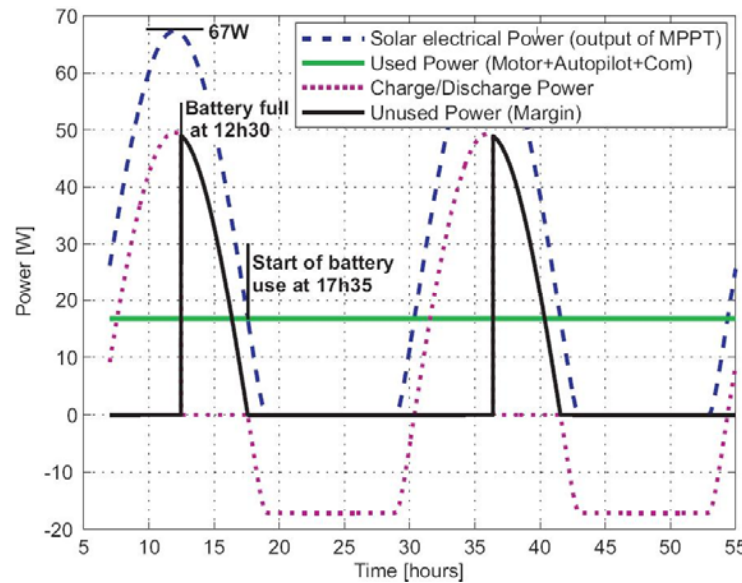
Sky-Sailor Design

- Meth. Application
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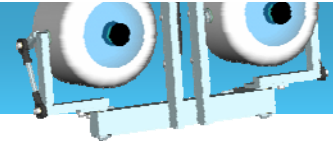
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Sky-Sailor Prototype



Introduction

Design Methodology

Sky-Sailor Design

Sky-Sailor Prototype

- Config & Structure
- Aerodynamics
- Solar Generator
- Propulsion
- Autopilot
- Modeling & Control
- Experiments

Scaling

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Sky-Sailor Prototype

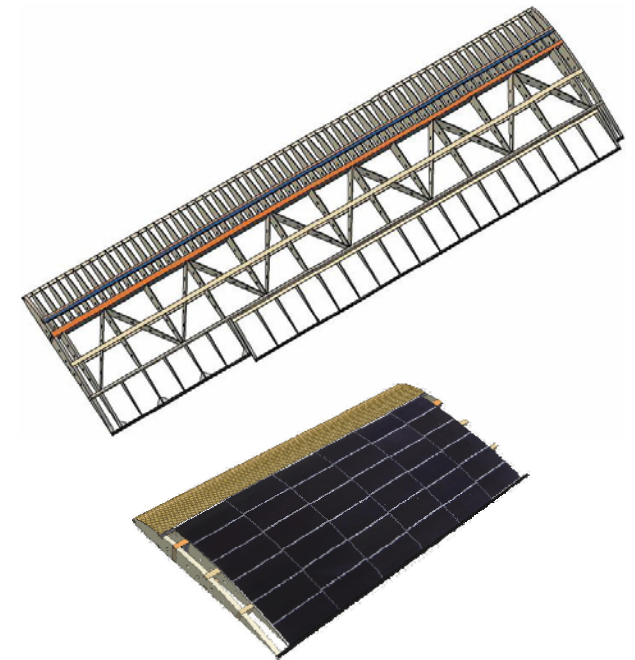
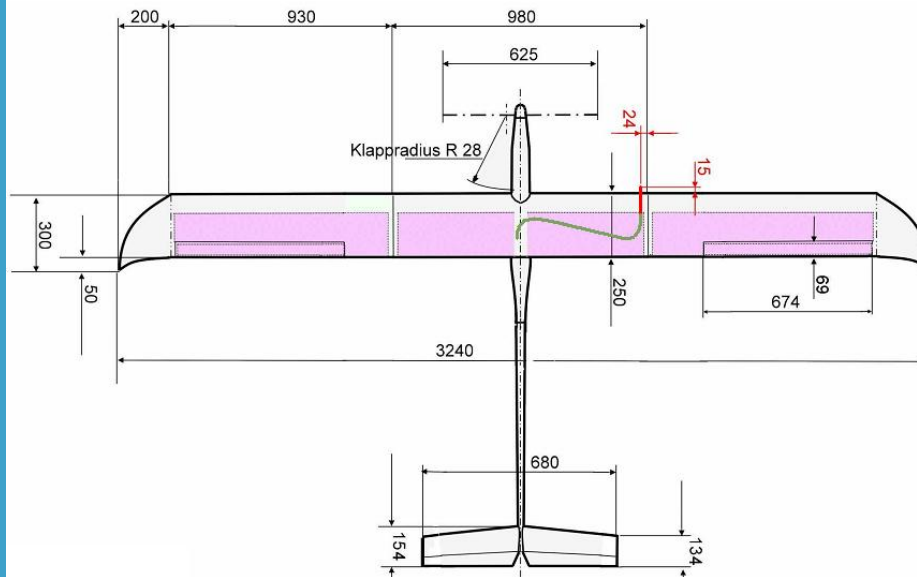


Configuration

3 axis glider, V-tail, constant chord
Adapted from « Avance » record airplane of W. Engel
Naturally stable

Structure

Composite materials (Carbon, Aramide, Balsa)
Spar-Ribs construction method
Wingspan 3.2 m
Surface 0.776 m²
Empty Weight 0.725 kg



Introduction

Design Methodology

Sky-Sailor Design

Sky-Sailor Prototype

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Dedicated Airfoil **we3.55-9.3**

Nominal flight speed	8.4 m/s
Nominal flight power (2.55 kg)	9 W
Glide ratio	23.5
Vertical glide speed	0.35 m/s

Introduction

Design Methodology

Sky-Sailor Design

Sky-Sailor Prototype

- Config & Structure
- **Aerodynamics**
- Solar Generator
- Propulsion
- Autopilot
- Modeling & Control
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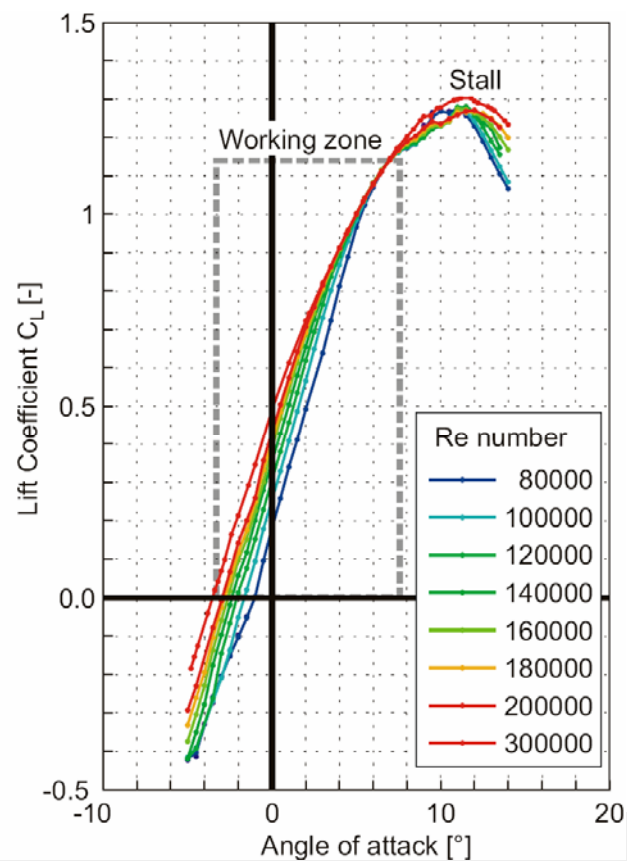
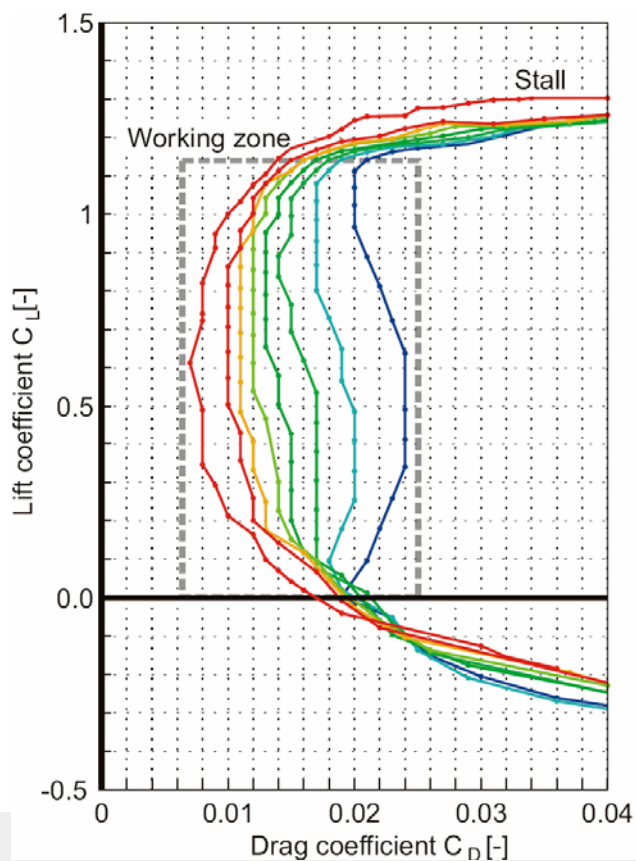
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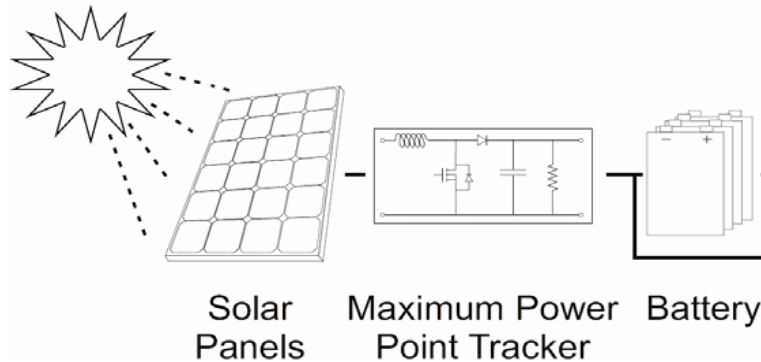


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Solar Generator



Introduction

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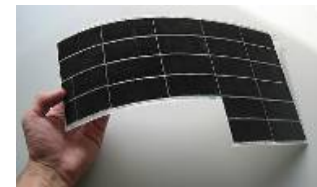
- Config & Structure
- Aerodynamics
- Solar Generator
- Propulsion
- Autopilot
- Modeling & Control
- Experiments

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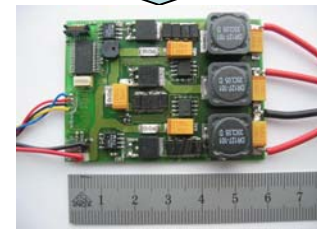
216 RWE solar cells (17% eff, ~90 W max)

- encapsulated into 3 solar panels
- non reflective encapsulation



Maximum Power Point tracker

- 97 % efficiency for 25 g and 90 W



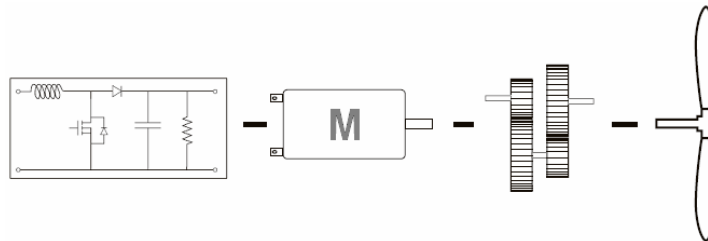
Lithium-Ion battery

- 250 Wh, 1.056 kg → 240 Wh/kg
- cycle efficiency 94.8 %



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Introduction

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Sky-Sailor Design

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- Config & Structure
- Aerodynamics
- Solar Generator
- **Propulsion**
- Autopilot
- Modeling & Control
- Experiments

Scaling

Conclusion

High efficiency Propeller from E. Schöberl

- 60 cm diameter
- Carbon
- 85.6 % efficiency

➔ Program created to select the best motor & gearbox combination out of 2600 motors

Gearbox

- Spur gearhead, own development

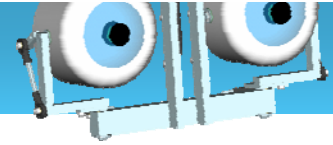
Brushless Motor (LRK Strecker)

- 86.8% efficiency
- Excellent cooling
- Low weight

Jeti Advance 45 Opto Plus brushless controller



Autopilot



- Special needs (solar panels monitoring,...)
- Extreme weight & power constraints
- ➔ Own Control & Navigation System

Link to videos:

<http://www.sky-sailor.ethz.ch/videos.htm>

Introduction

Design Methodology

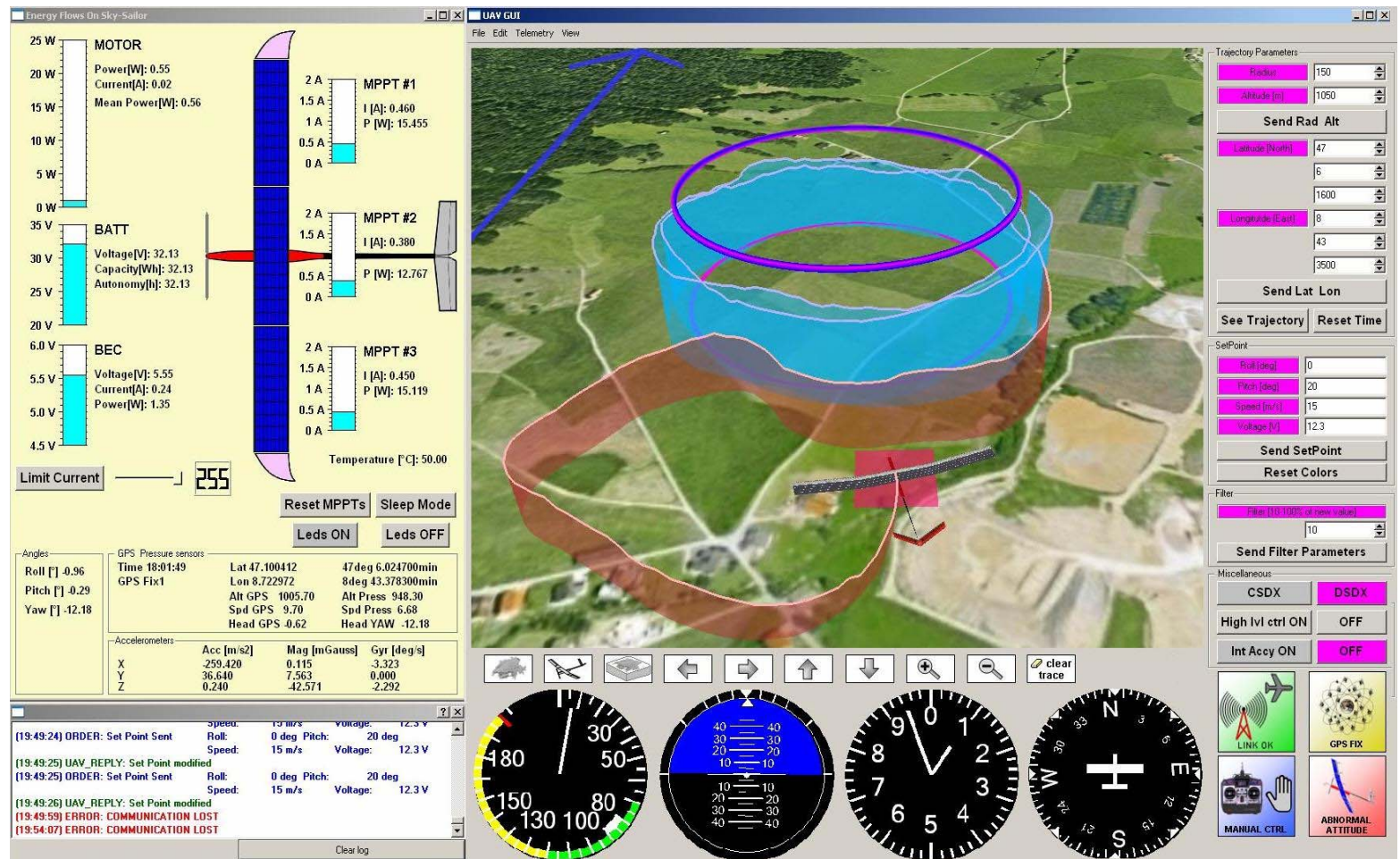
Sky-Sailor Design

Sky-Sailor Prototype

- Config & Structure
- Aerodynamics
- Solar Generator
- Propulsion
- Autopilot
- Modeling & Control
- Experiments

Scaling

Conclusion



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Goals

- Tune controller parameters
- Test Navigation algorithms
- Evaluate airplane capabilities

Introduction

Design Methodology

Sky-Sailor Design

Sky-Sailor Prototype

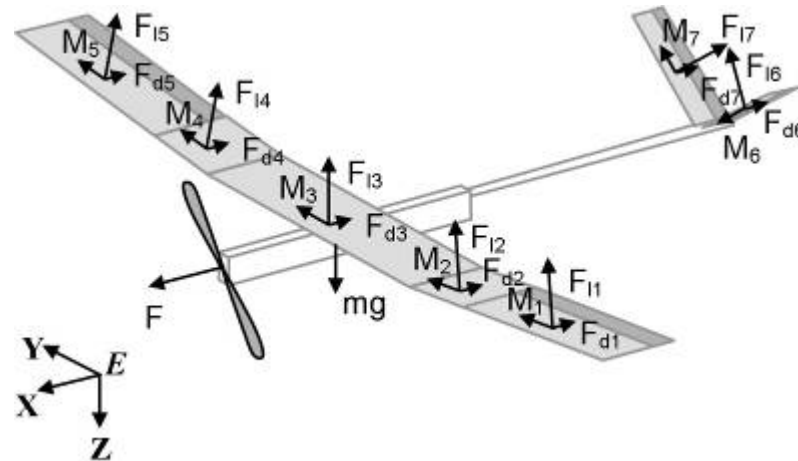
- Config & Structure
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$$F_{tot} = F_{prop} + \sum_{i=1}^7 F_{Li} + F_{di}$$

$$M_{tot} = \sum_{i=1}^7 M_i + F_{Li} \times r_i + F_{di} \times r_i$$



$$F_{prop} = f(\dot{x}, U_1)$$

$$F_{li} = C_{li} \frac{\rho}{2} S_i v^2$$

$$F_{di} = C_{di} \frac{\rho}{2} S_i v^2$$

$$M_i = C_{mi} \frac{\rho}{2} S_i v^2 \cdot chord_i$$

$$\begin{bmatrix} C_{l1} & C_{d1} & C_{m1} \end{bmatrix} = f(Aoa_1, U_2)$$

$$\begin{bmatrix} C_{li} & C_{di} & C_{mi} \end{bmatrix} = f(Aoa_i) \quad \text{for } i=2,3,4$$

$$\begin{bmatrix} C_{l5} & C_{d5} & C_{m5} \end{bmatrix} = f(Aoa_5, U_3)$$

$$\begin{bmatrix} C_{l6} & C_{d6} & C_{m6} \end{bmatrix} = f(Aoa_6, U_4)$$

$$\begin{bmatrix} C_{l7} & C_{d7} & C_{m7} \end{bmatrix} = f(Aoa_7, U_5)$$



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Experiments

Introduction

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Sky-Sailor Design

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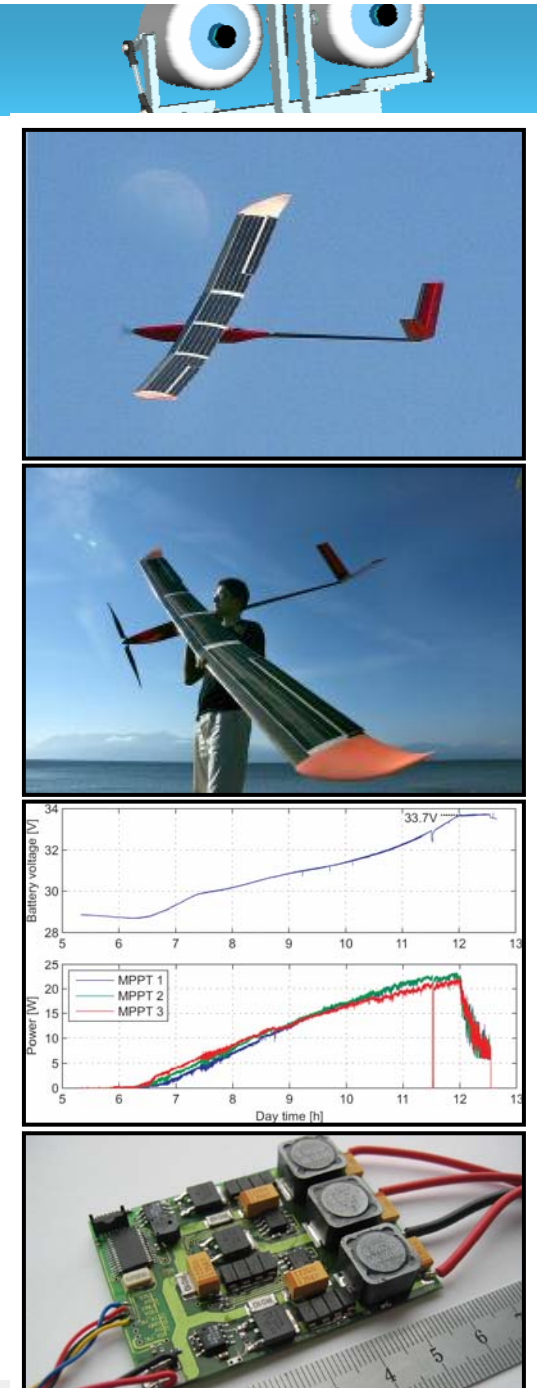
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- **Several tests with subgroups**
 - Efficiencies increase
 - Weight reduction
 - Adding functionalities
 - Safety increase
- **Flight tests with a non-solar proto**
 - Aerodynamics validation
 - Power consumption verification
 - Autopilot electronic tests
 - Control & Navigation tuning
- **Flight tests with the Sky-Sailor**
 - Solar charge
 - Long flights (>3h)
 - 24 hours flight

Flight videos:

<http://www.sky-sailor.ethz.ch/videos.htm>



27 hours flight, 21st of June 2008



Introduction

Design Methodology

Sky-Sailor Design

Sky-Sailor Prototype

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- Aerodynamics
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- Experiments

Scaling

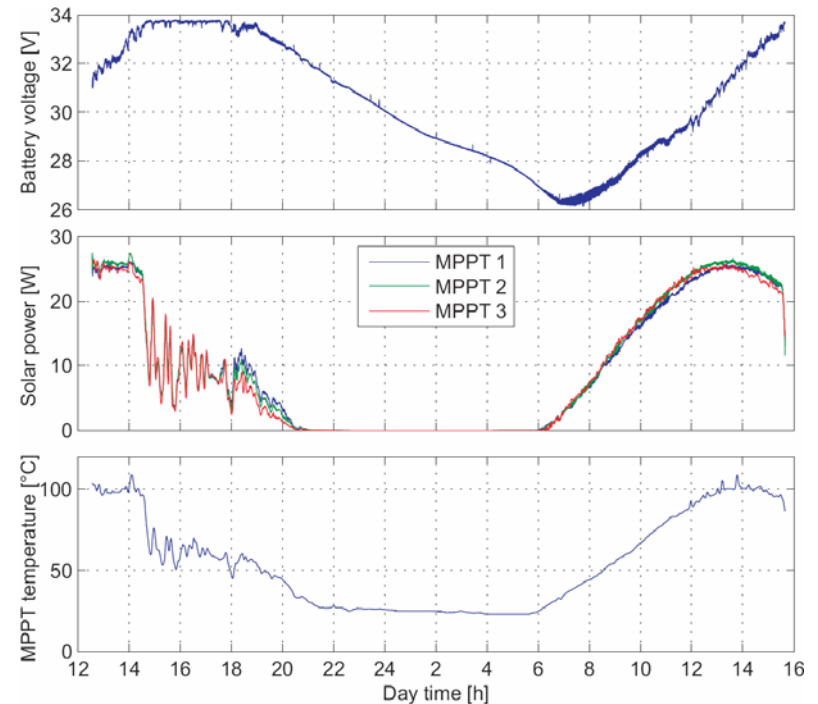
Conclusion

Conditions

- Excellent irradiance
- Bad wind conditions → more power needed during the day

Achievements

- Duration: 27h05
- Distance: 874 km
- Av. speed: 8.4 m/s
- Mean power: 23+1.9W
- E_{used} : 675 Wh
- E_{obtained} : 768 Wh



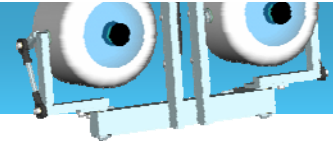
→ Continuous flight proved to be feasible without thermic or altitude gain



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Scaling & Other considerations



Introduction

Design Methodology

Sky-Sailor Design

Sky-Sailor Prototype

Scaling

- Down: MAV
- Up: Manned & Hale
- Epot & Thermal

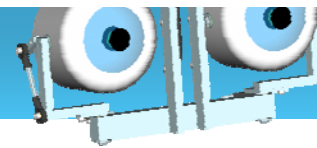
Conclusion



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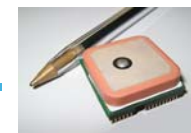
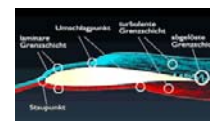
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Down Scaling



Drawbacks

- Efficiency of propulsion group ↘
- At low power, DC motor but no BLDC
- Efficiency of aerodynamic ↘ (low Re)
- Servos below 5 grams → poor quality
- High E_{density} batt not easily scalable
- Autopilot sensors limited (due to weight, ex: no tiny GPS or IMU)
- Silicon solar cells scale in 2D (not 3D)
 - Not flexible for low radius
 - Weight percentage ↗
- MPPT efficiency ↘ ($V_{\text{diode loss}}/V_{\text{MPPT}}$ ↗)



→ No 24h solar flight at MAV size, but day flight possible

Introduction

Design Methodology

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Sky-Sailor Prototype

Scaling

- Down: MAV
- Up: Manned & Hale
- Epot & Thermal

Conclusion



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Up Scaling



Introduction

Design Methodology

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Scaling

- Down: MAV
- Up: Manned & Hale
- Epot & Thermal

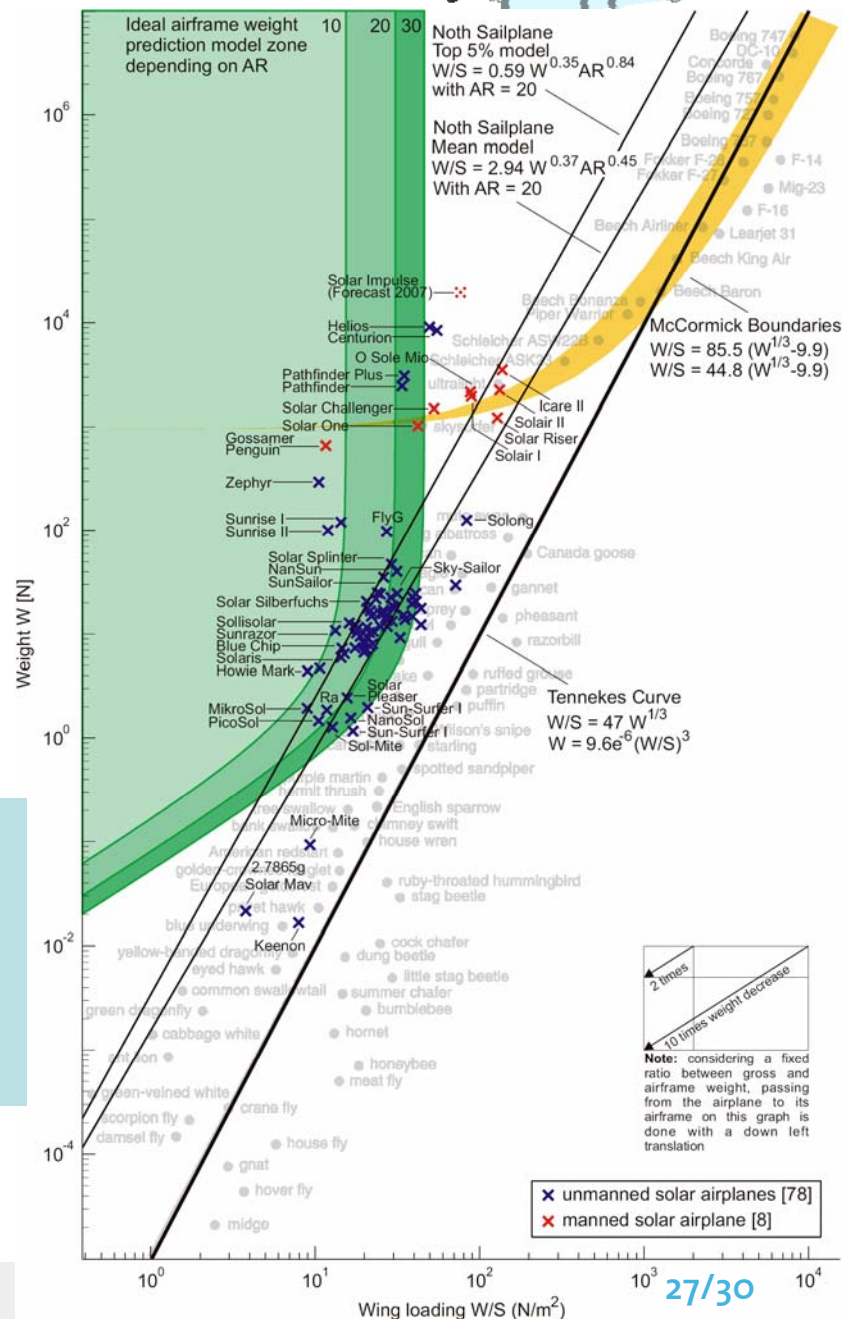
Conclusion

Drawback

- Structure weight $\sim b^3$
- Theory said it should be $\sim b^2$
- ➔ The bigger they are, the lighter the construction method has to be
- ➔ Fragility & Risks

➔ Continuous flight possible only for 1 or 2 passengers but...

- ➔ Low speed (long flights)
- ➔ No comfort possible



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Two possibilities to increase flight endurance are:

- Use of altitude to store energy
 - + less battery needed
 - altitude varies → aerodynamics not optimized for a fixed density
- Thermal soaring
 - + free climbing, save energy
 - require a method to detect & soar thermal

Introduction

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Scaling

- Down: MAV
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- Epot & Thermal

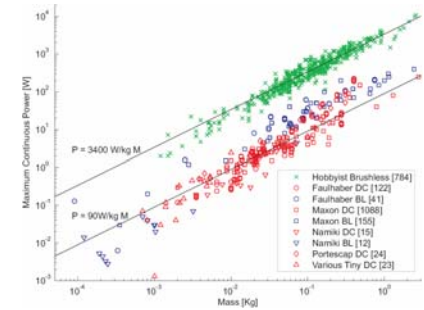
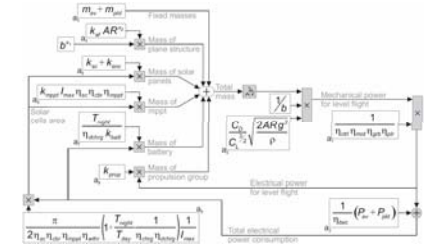
Conclusion



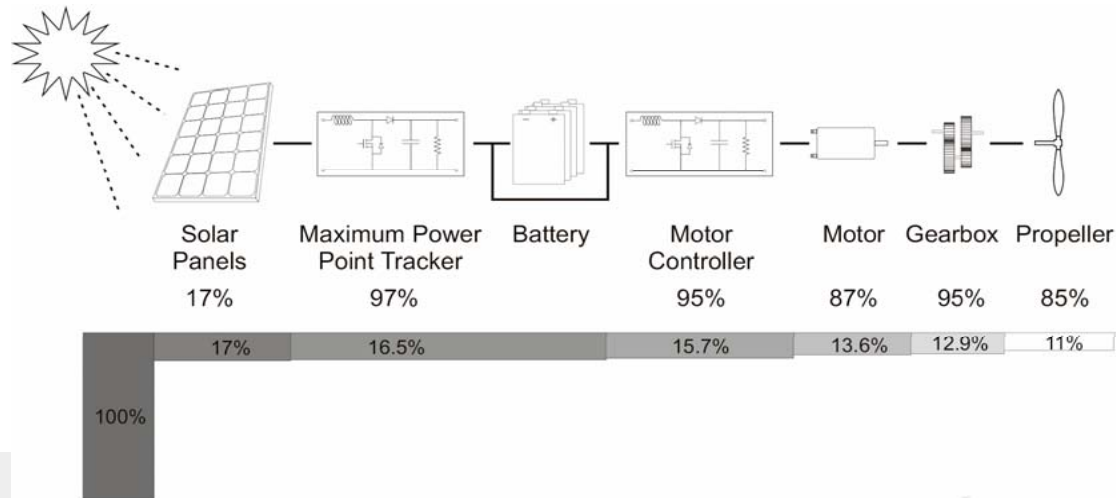
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Conclusion



- **Methodology developed**
 - Simple and versatile
 - Valid on a large range
 - Solid weight & efficiency models
 - Allows fast feasibility studies
 - Allows to identify bottle necks
- **Prototype built**
 - Validation of the design
 - Continuous flight proven
 - Very good know-how acquired



Introduction

Design Methodology

Sky-Sailor Design

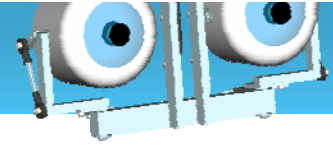
Sky-Sailor Prototype

Scaling

Conclusion



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Introduction

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Sky-Sailor Design

Sky-Sailor Prototype

Scaling

Conclusion

- **Scaling problems**
 - Down: efficiencies and aerodynamics
 - Up: large wing structure
- **Outlook**
 - Increase # parameters (efficiency = $f(\text{power})$)
 - Flight algorithm learning energy saving
 - Thermal soaring
 - Building: improve costs, time & robustness



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Future of solar aviation



Introduction

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Scaling

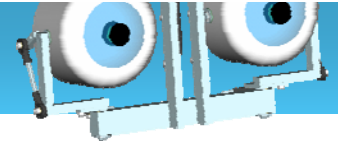
Conclusion

- **MAV size**
 - Needs still many improvements (eff, aerodynamics, batteries)
- **At 2-10 meters**
 - Forest fire monitoring
 - Pipeline surveillance
 - ...
 - ➔ In 10 years with tech. improvements (batteries, solar cell)
- **HALE**
 - Act as mobile phone antenna
 - Real need to stay airborne
 - ➔ Will require many improvements (structure, batteries)
- **Manned airplane (transportation)**
 - High fragility, risks and long trips
 - Even with a 100% eff. airplane, problem is the sun!
 - ➔ A better idea would be to:
 - ➔ Transform E_{solar} on the ground ➔ H₂
 - ➔ Use H₂ in flight (fuel cell & electrical motor)



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Thank you for your attention

Questions ?

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Scaling

Conclusion

Special Thanks to:

- **Prof. Siegwart and the entire ASL**
- **Walter Engel & all the people who worked on the project**
- **Doctoral comity**



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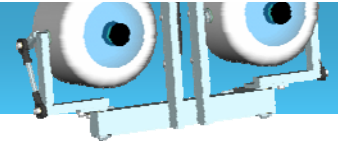
Conclusion

- **Solar Generator**
 - [Spectrum, Albedo, Sun angle](#)
 - [T_{day} & I_{max}](#)
 - [Best research cell efficiencies](#)
 - [I-V curve](#)
 - [MPPT](#)
 - [Integration in the wing](#)
- **Energy Storage**
 - [All solutions](#)
 - [Energy density of fuel](#)
 - [Lithium-Ion battery evolution](#)
- **Propulsion Group**
 - [Motors](#)
 - [Propeller](#)
 - [Weight prediction models](#)
- **Autopilot**
 - [Schematic](#)
 - [Telemetry](#)
 - [Power consumption](#)
 - [Placement](#)
 - [GUI \(thermals\)](#)
 - [Simulation & modeling](#)
- **Overall**
 - [Energy Chain](#)
 - [Solar Airplane: light and slow](#)
 - [Weight-Power-Autonomy](#)
 - [Methodology Resolution](#)
 - [30 Parameters](#)
 - [Weight distribution](#)
- **Applications**
 - [Potential applications](#)
 - [Sky-Sailor](#)
 - [MAV](#)
 - [Manned](#)
 - [HALE](#)
 - [Mars](#)
- **Other**
 - [Using thermals](#)
 - [Sun Surfer](#)
 - [Design phases](#)
 - [Airframe model](#)
 - [27 hours flight](#)



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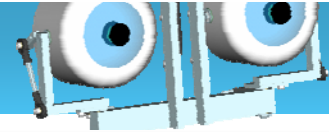
Solar Generator



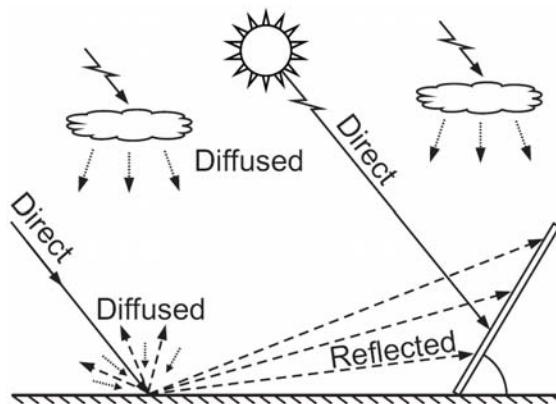
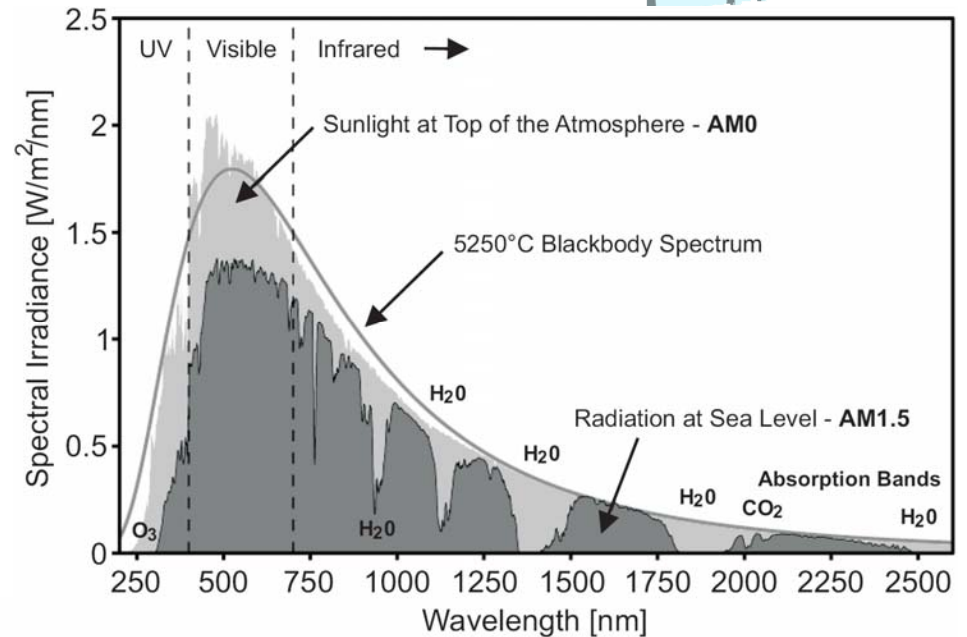
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Solar Energy

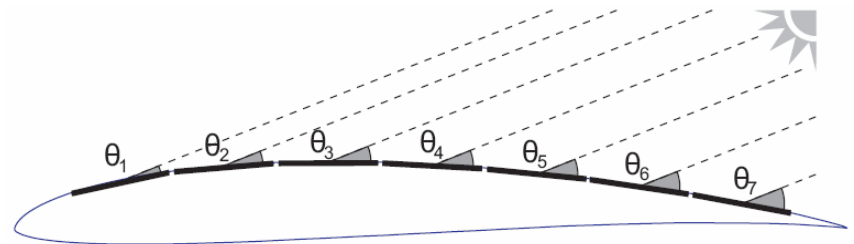


Solar Spectrum

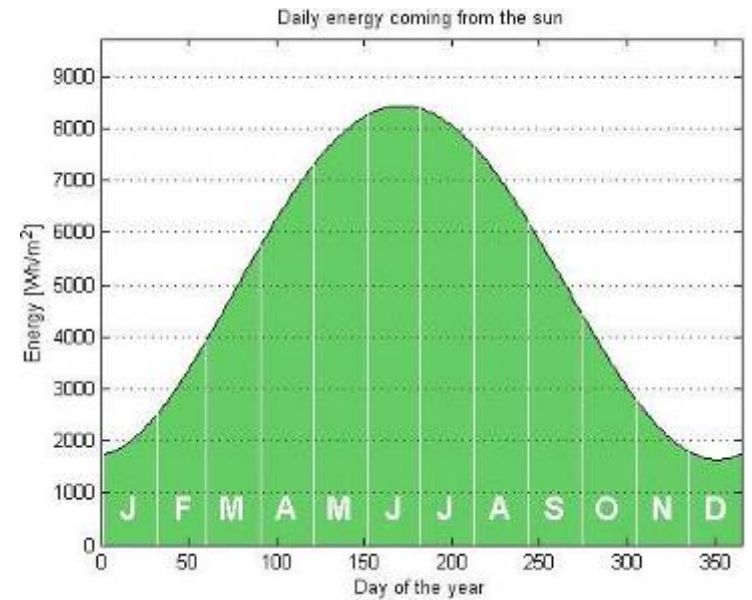
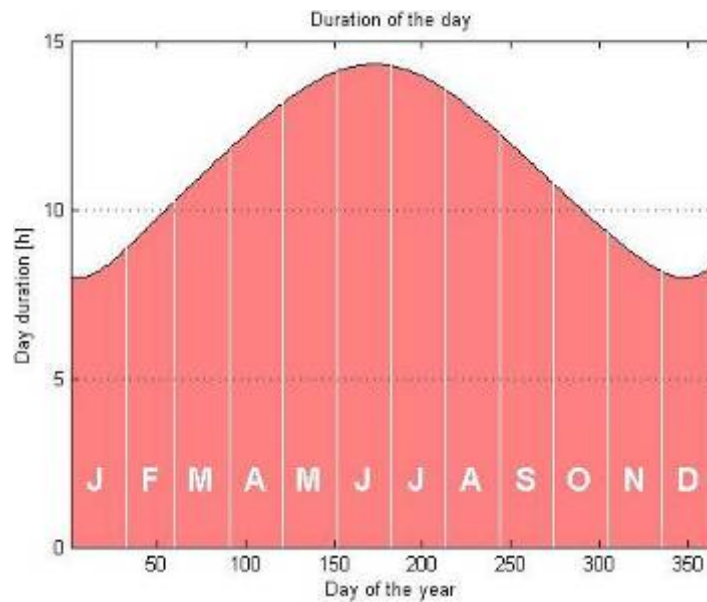
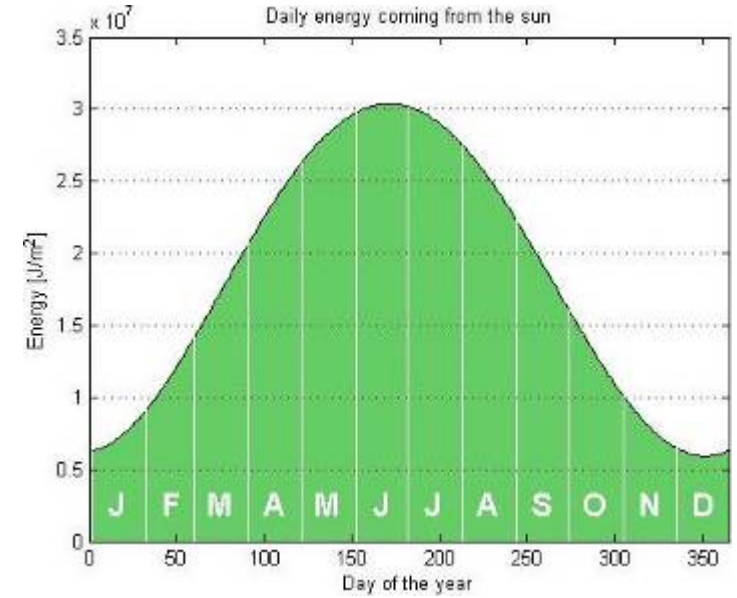
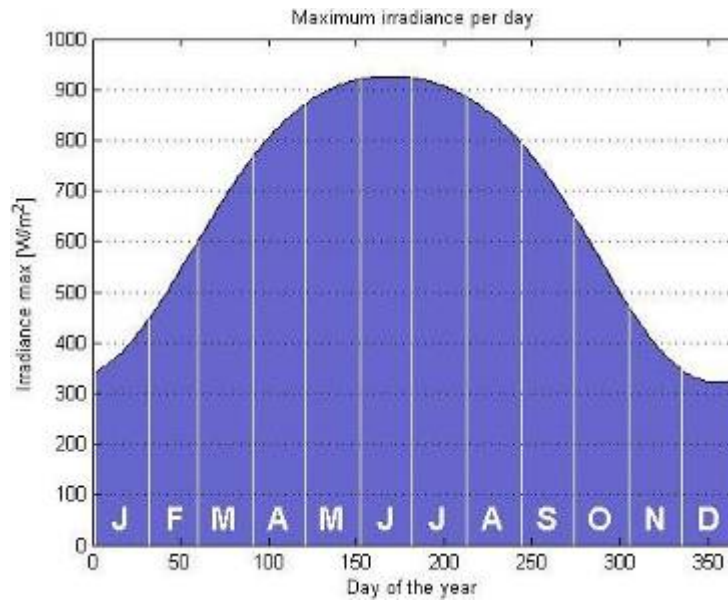
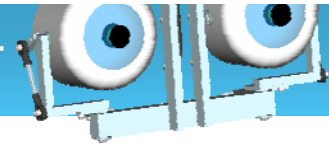


Direct, diffused and reflected light

Angle of incidence variation



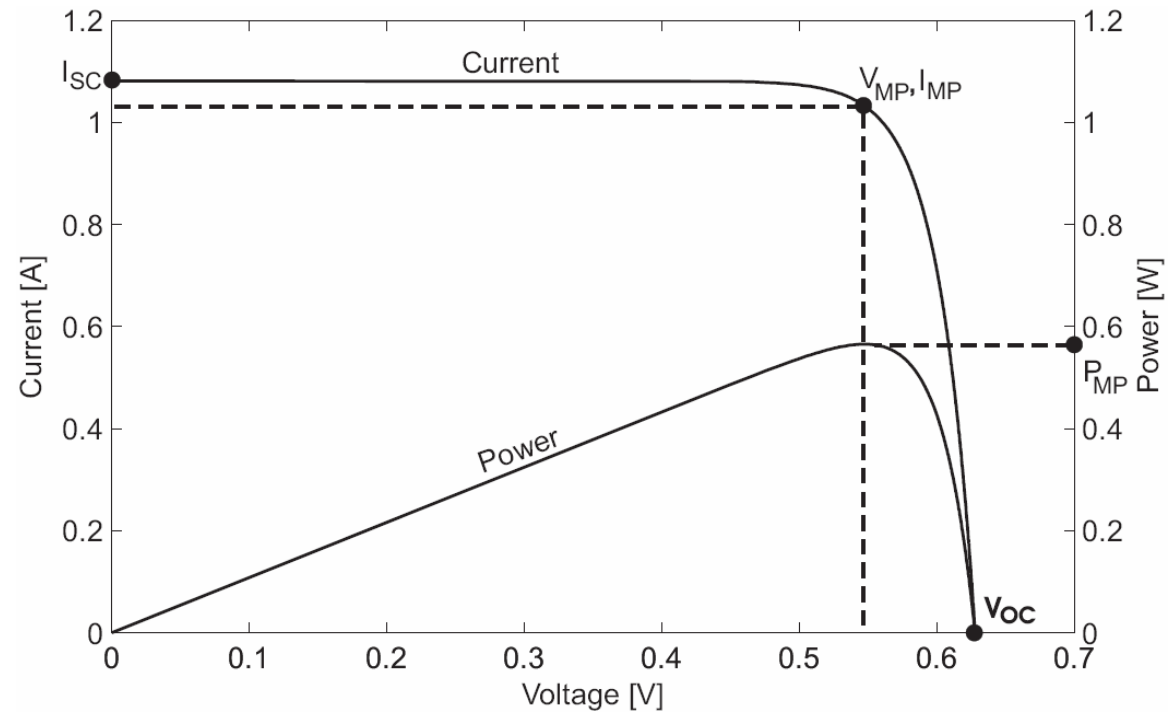
Variation of T_{day} and I_{max} along year



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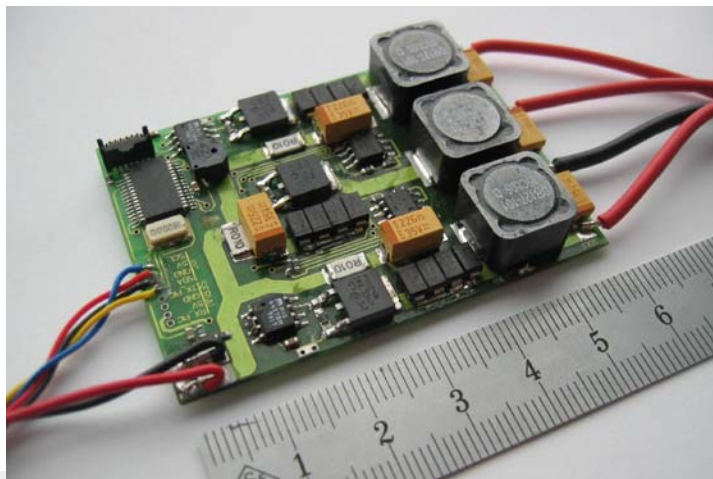
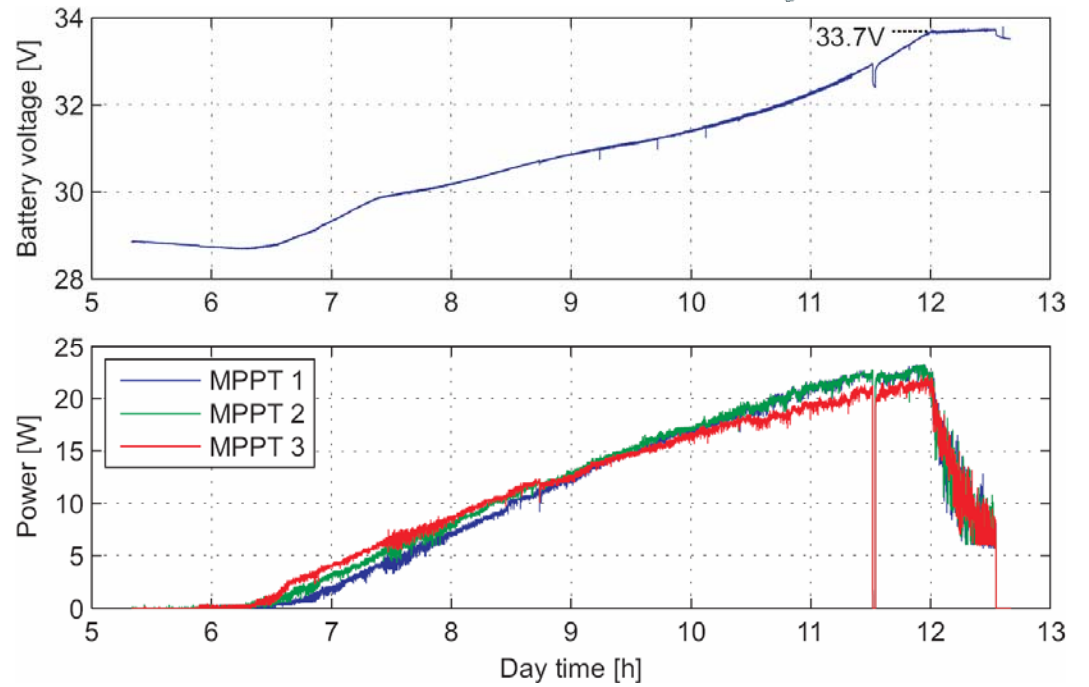
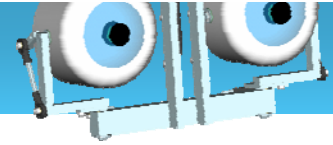
Solar Cell



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MPPT

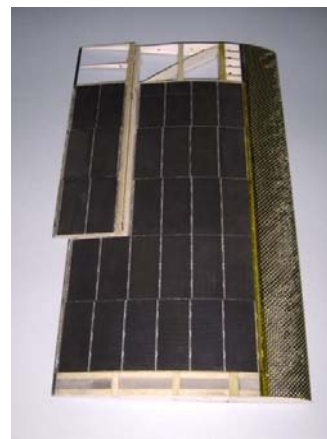
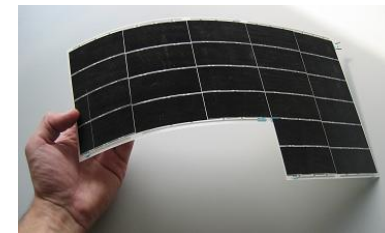
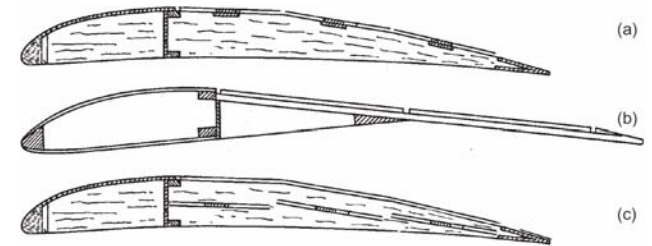
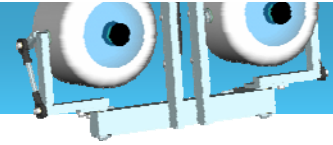


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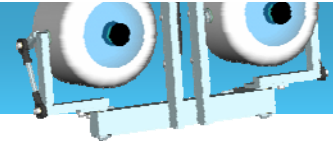
Solar cells integration

Structure



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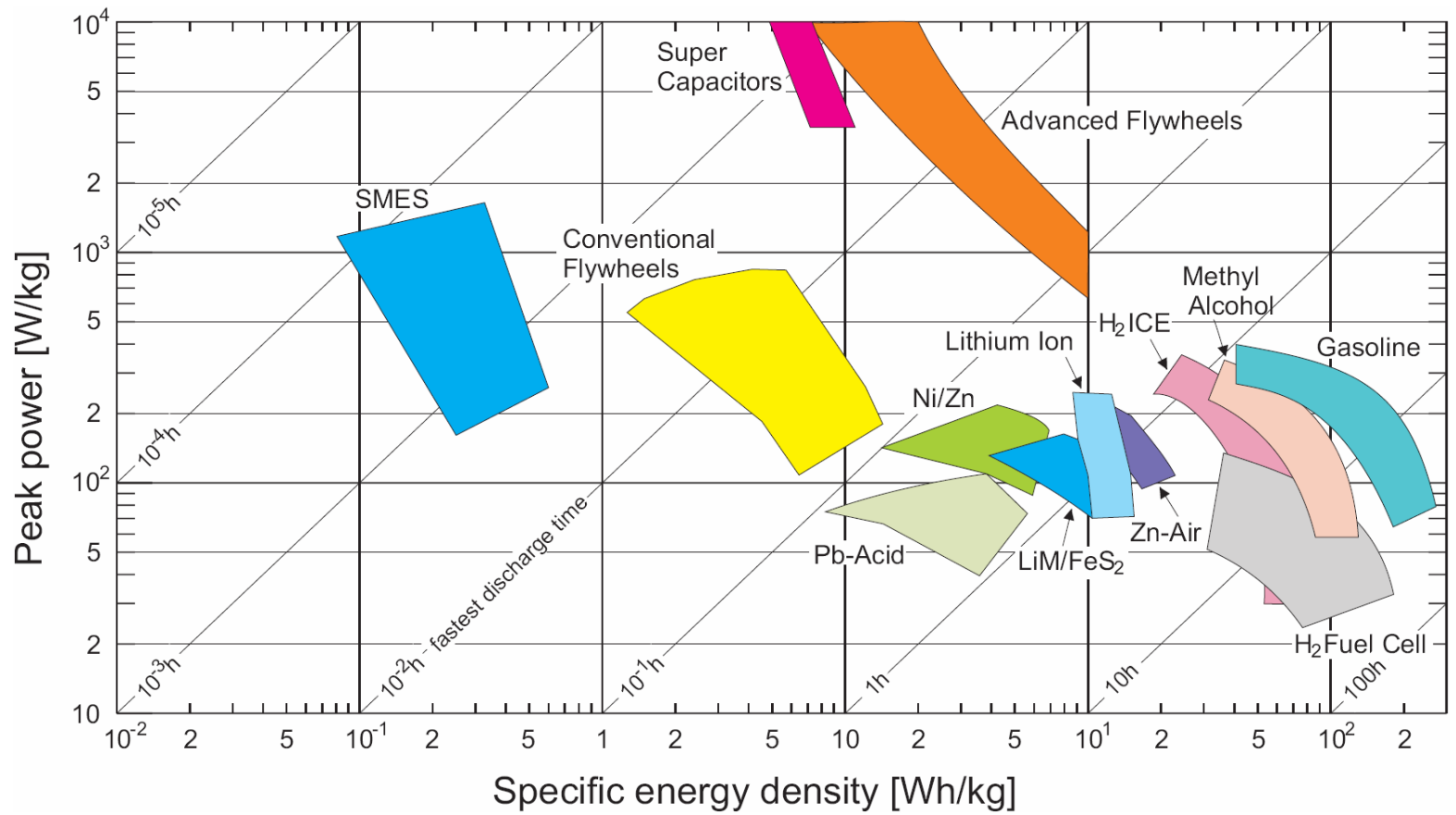
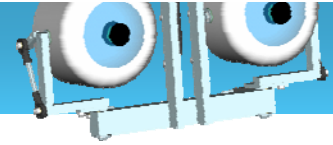
Energy Storage



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Energy storage solutions



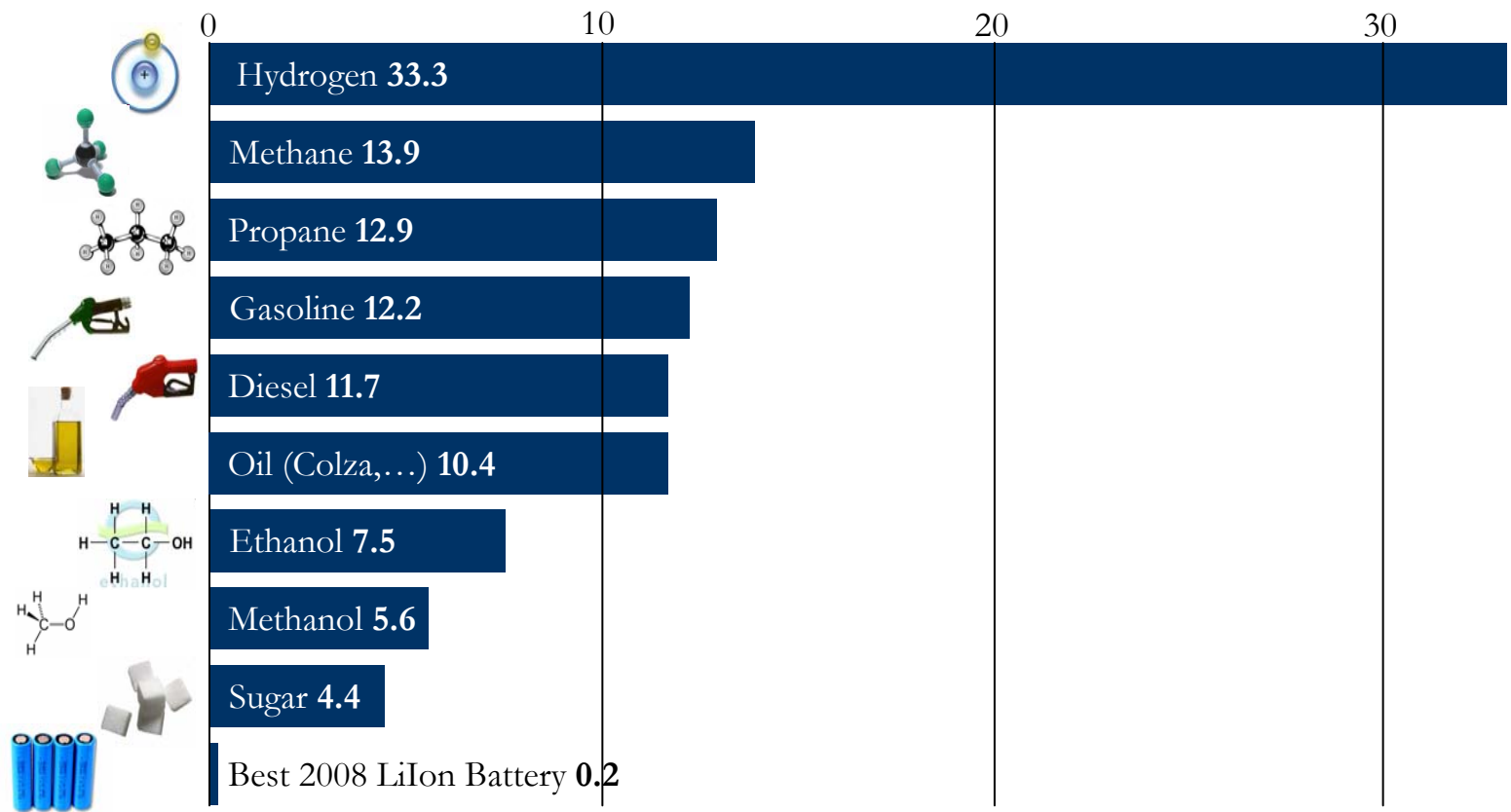
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Energy Storage



Energy density of some reactants [kWh/kg]
(LHV Lower heating value)

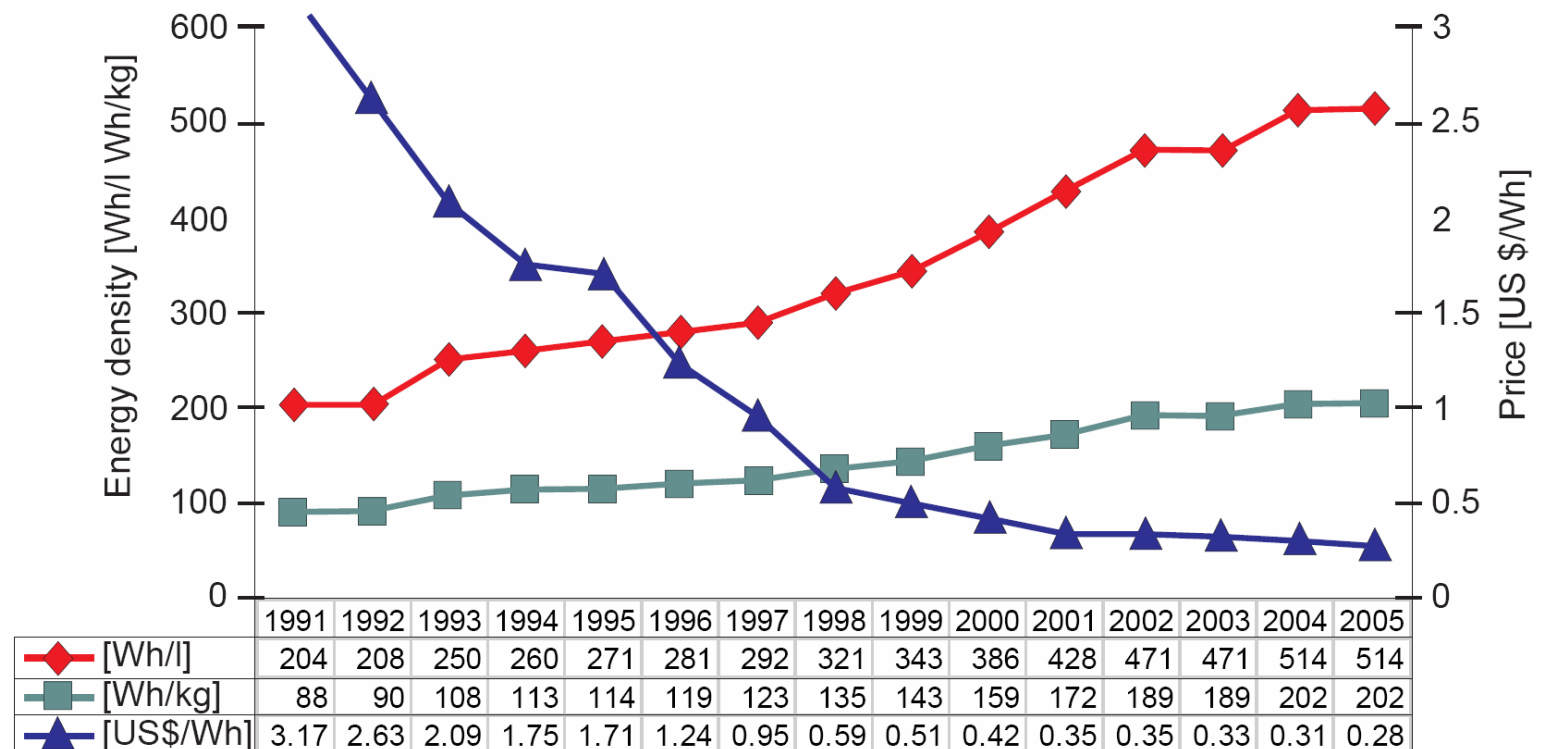


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➔ Important to keep in mind Availability / Efficiency of converters

Lithium-Ion battery evolution

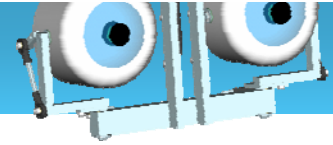


Energy density + 6.6%/year
Price - 17%/year



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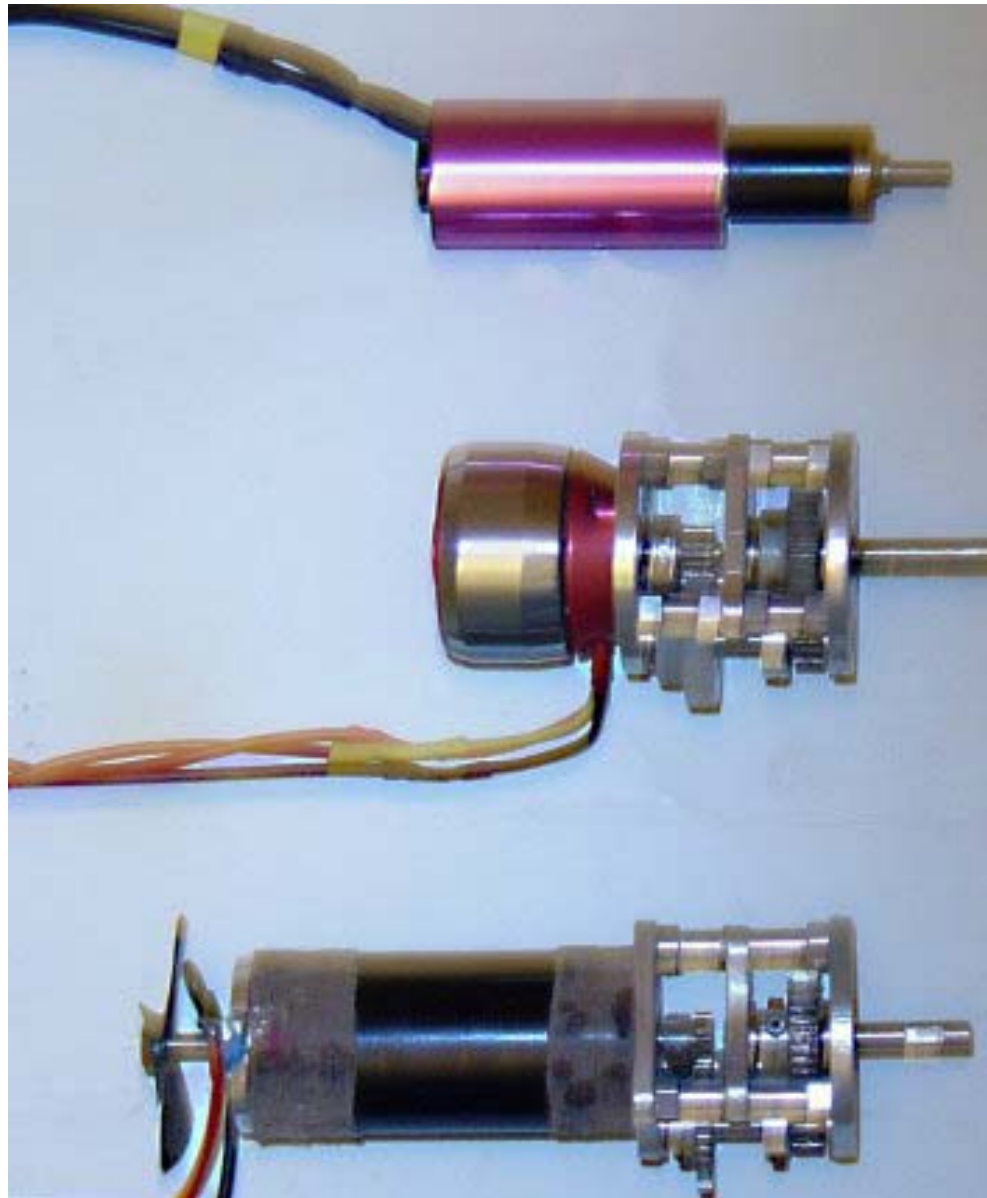
Propulsion Group



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Motors



Brushless Innenläufer
Hacker B20-76L (2Pol)
Planetengetriebe 16:1

Gewicht 72g

Brushless LRK
Srecker228,10 (40Wdg;
16 Pol)
2-Stufengetriebe 9:1

Gewicht ca.90g

Glockenankermotor
MAXON DC RE 25, 20W
2-Stufengetriebe 8,08:1

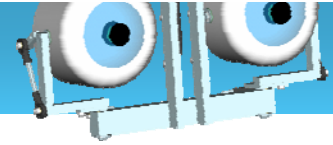
Gewicht156 g



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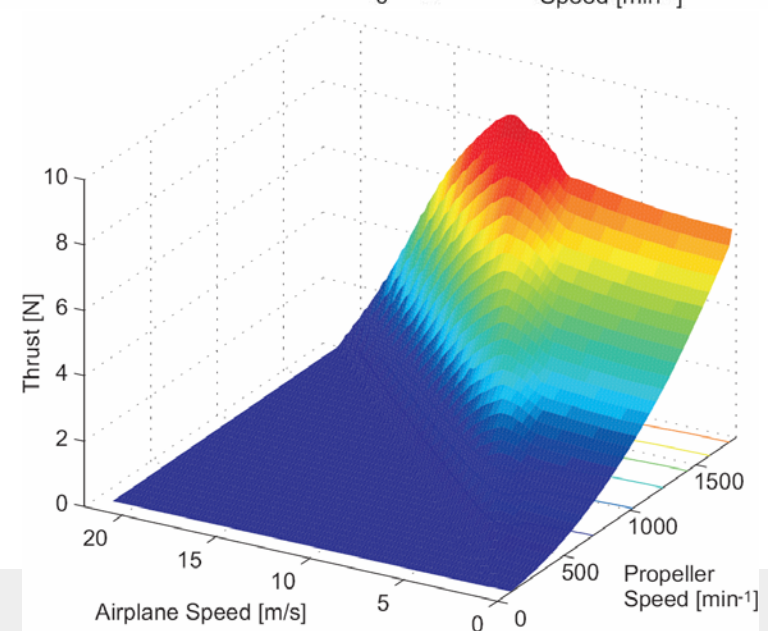
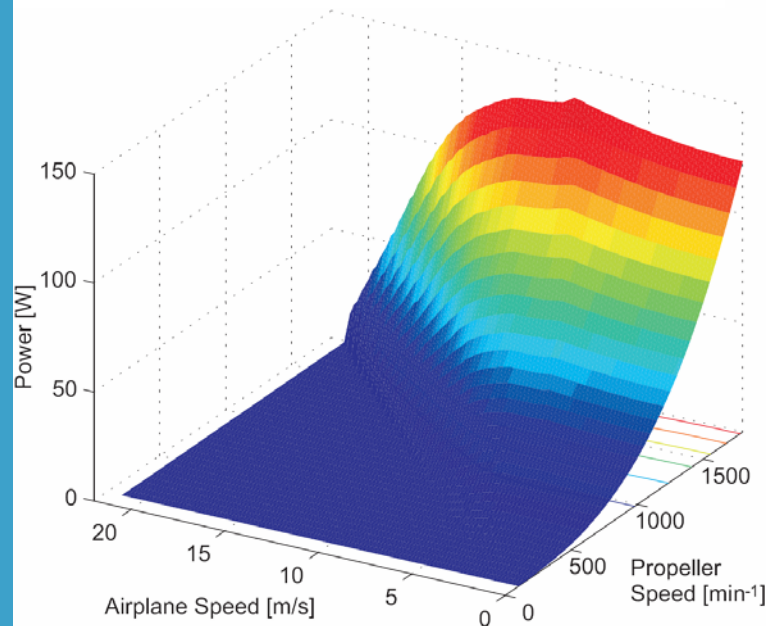
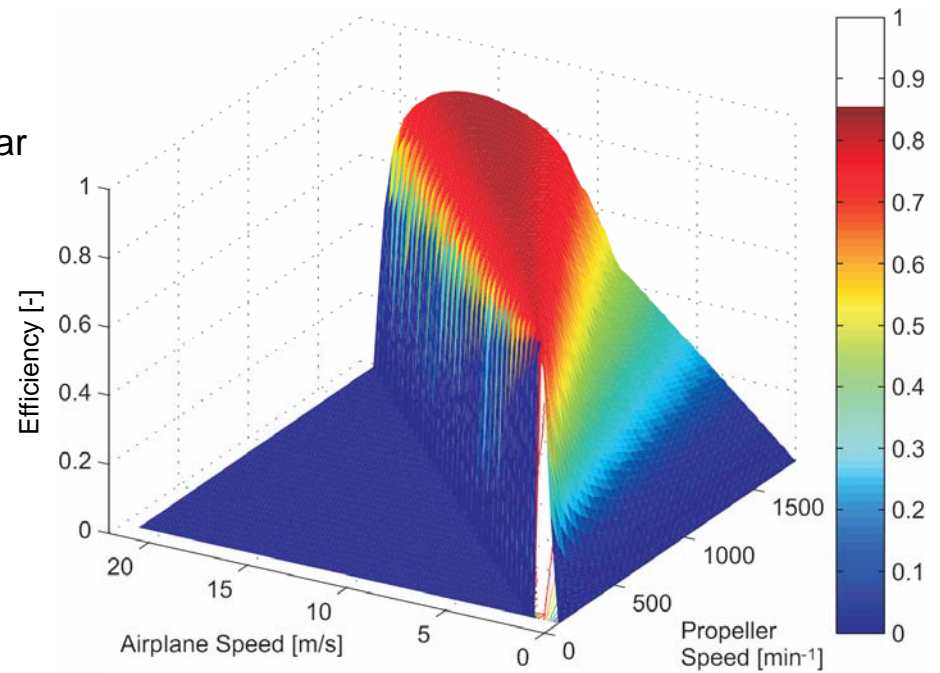
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Propeller



Designed by E. Schöberl

- « Master of Prop »
- Also worked on Icaré and other solar airplanes



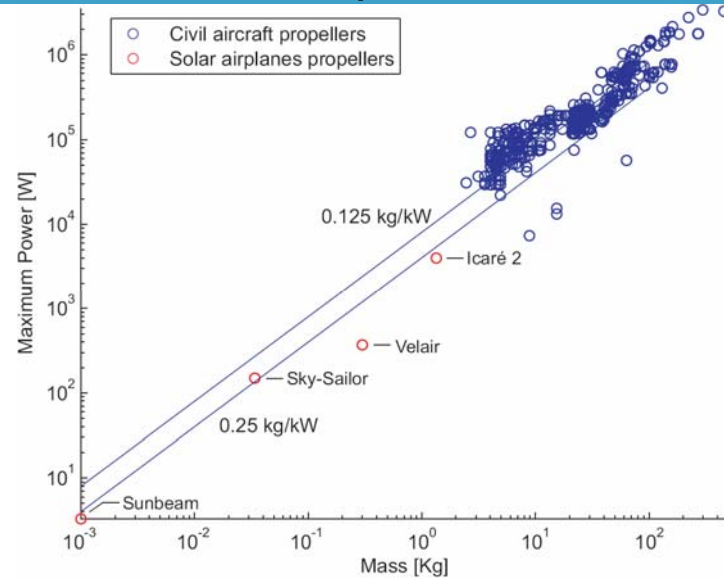
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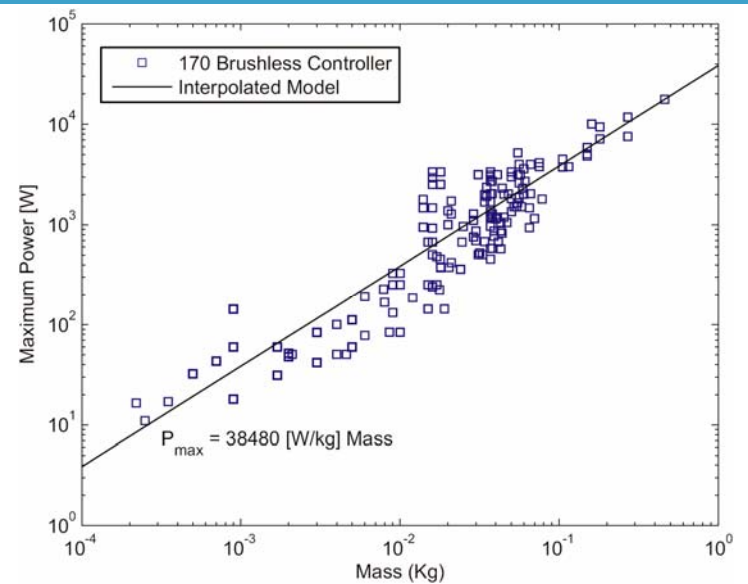
Weight prediction models



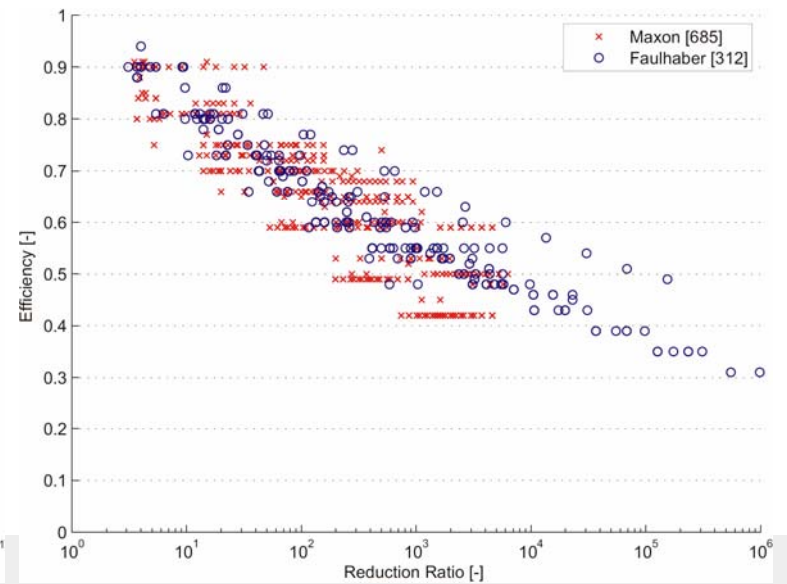
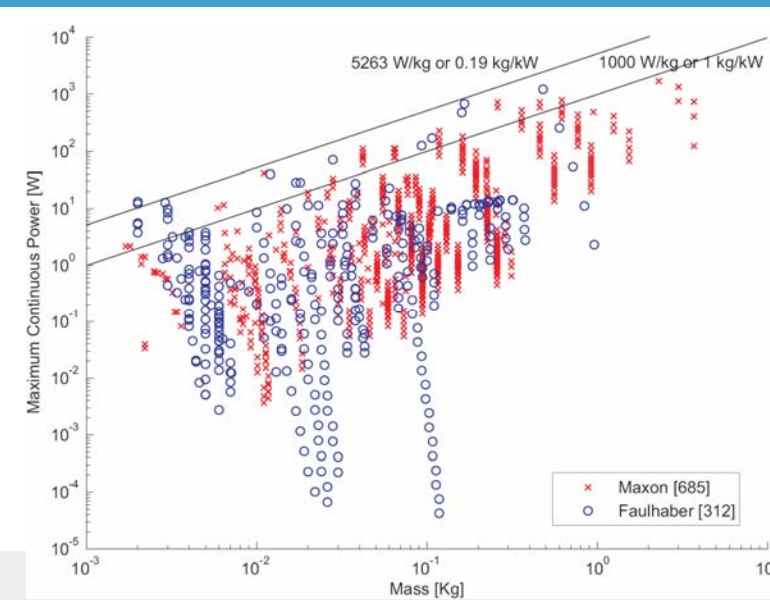
Propellers

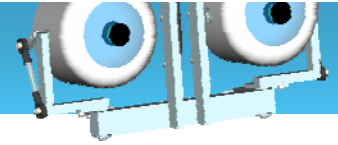


Brushless controllers



Gearboxes





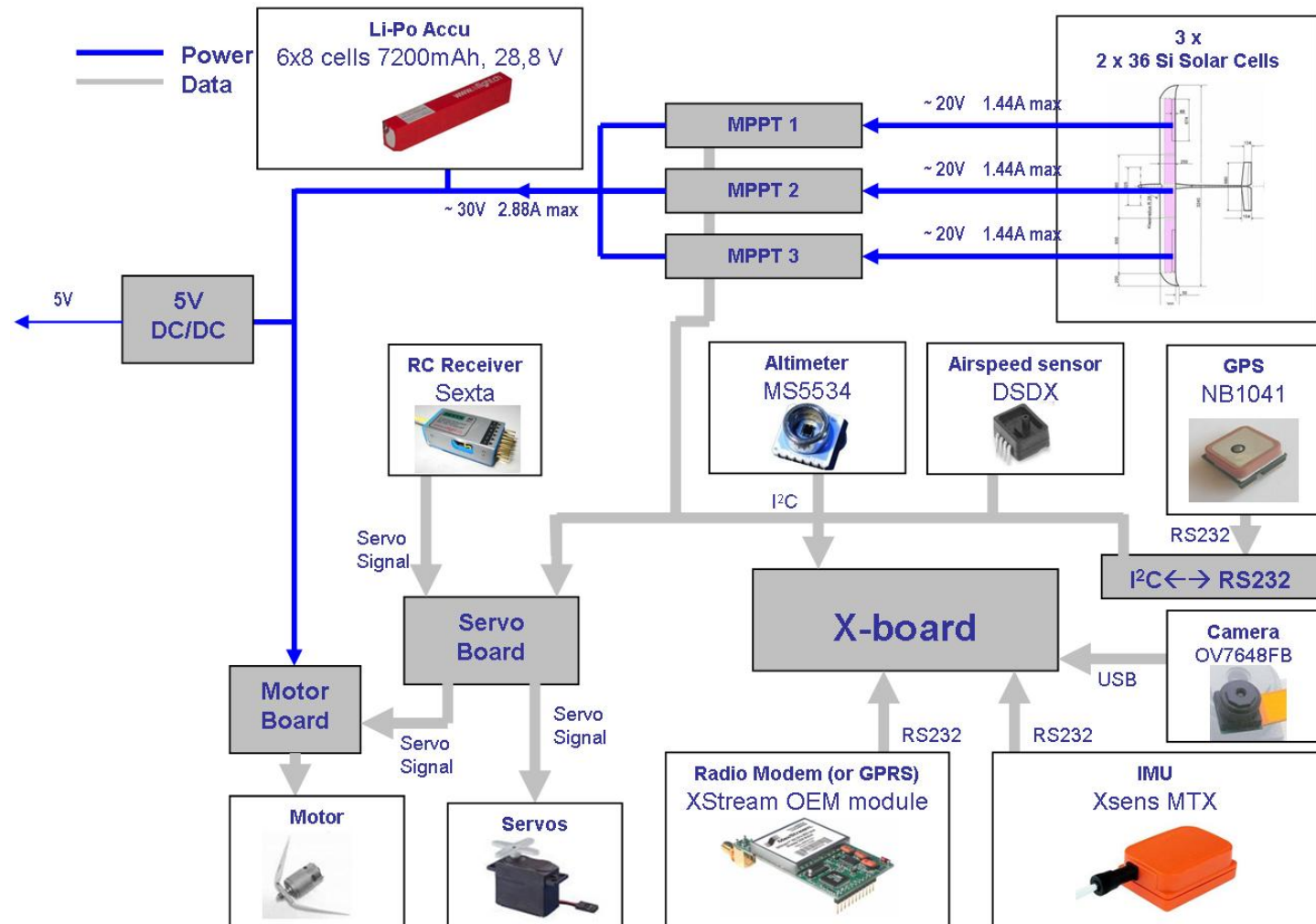
Autopilot



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Autopilot overview



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Telemetry



Autopilot V2 Electric Schematic & Registers v 7.0

Power

- Ground
- Battery V+ [24-33.7V]
- Bec V+ [5.6 V]

Digital Electronics

- Ground
- 5V regulated
- 3.3V regulated
- I²C clock line (SCL)
- I²C data line (SDA)
- Other data line (PPM, RS232)

Sky-Sailor Project, A. Noth, Jan 2007

Module address	(0x50 in PicWatch)
0x22	r MPPT Temperature1 [°C]
0x23	r MPPT Tempertaure2 [°C]
0x24	r Current MPPT 1 [1/100 A]
0x25	r Current MPPT 2 [1/100 A]
0x26	r Current MPPT 3 [1/100 A]
0x27	r Voltage lsb [1/1000 V]
0x28	r Voltage msb [1/1000 V]
0x29	r/w Working Mode
	10 - sleep mode (0x0A)
	11 - track mode (0x0B)
	12 - reset mode (0x0C)
0x2A	r/w Duty Cycle MPPT 1 []
0x2B	r/w Duty Cycle MPPT 2 []
0x2C	r/w Duty Cycle MPPT 3 []
0x2D	r/w Current limitation [1/100A]

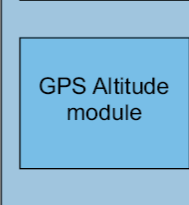
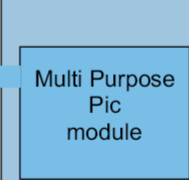
Module address	(0x30 in PicWatch)
0x22	r Pressure lsb [Internal Unit]
0x23	r Pressure msb [IntU]
0x24	r Raw pressure lsb [IntU]
0x25	r Raw pressure msb [IntU]
0x26	r Pressure offset lsb [IntU]
0x27	r Pressure offset msb [IntU]
0x28	r Speed lsb [1/100 m/s]
0x29	r Speed msb [1/100 m/s]
0x2A	r/w Melody
	1 - waiting gps
	2 - gps fixed
	3 - Do-Re...Do
	4 - Music
	11-19 Warning nr 1-9
0x2B	r/w Reset Pressure 1 - reset 0 - else
0x2C	r/w Sensor Type
	10 - DSDX (0x0A)
	11 - CSDX (0x0B)

Module address	(25Hz) (0x40 in PicWatch)
0x22	r Voltage batt lsb [1/1000 V]
0x23	r Voltage batt msb [1/1000 V]
0x24	r Voltage bec lsb [1/1000 V]
0x25	r Voltage bec_m [1/1000 V]
0x26	r Current motor lsb [1/1000 A]
0x27	r Current motor msb [1/1000 A]
0x28	r Current servo lsb [1/1000 A]
0x29	r Current servo msb [1/1000 A]

Radio-Modem 900 Mhz

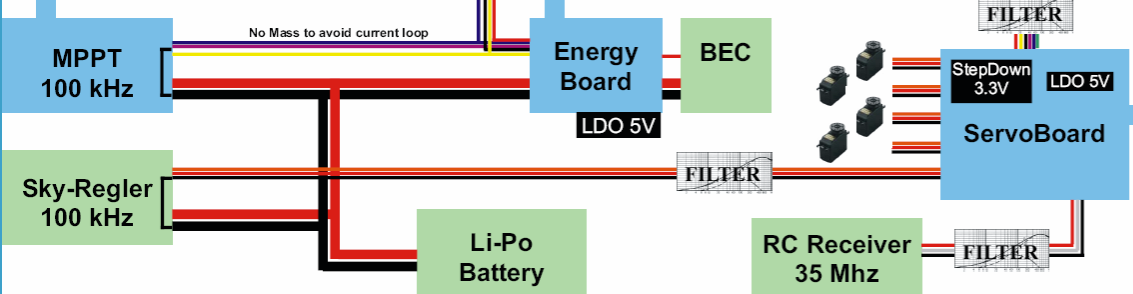


Autopilot Board



Module address	(0x20 in PicWatch)
0x22	r Pressure lsb [1/10 mbar]
0x23	r Pressure msb [1/10 mbar]
0x24	r Temperature lsb [1/10 °C]
0x25	r Temperature msb [1/10 °C]
0x26	r Altitude lsb [1/10 m]
0x27	r Altitude msb [1/10 m]
0x28	r Error
0x29	r Time hour [hr]
0x2A	r Time minute [min]
0x2B	r Time second [sec]
0x2C	r Latitude degree [deg]
0x2D	r Latitude minute [min]
0x2E	r Latitude 10000 th lsb [1/10000 min]
0x2F	r Latitude 10000 th msb [1/10000 min]
0x30	r Latitude direction [N/S]
0x31	r Longitude degree [deg]
0x32	r Longitude minute [min]
0x33	r Longitude 10000 th lsb [1/10000 min]
0x34	r Longitude 10000 th msb [1/10000 min]
0x35	r Longitude direction [E/W]
0x36	r Satellite fix 1=ok, no fix=0
0x37	r Number of satellite []
0x38	r Altitude GPS lsb [1/10 m]
0x39	r Altitude GPS msb [1/10 m]
0x3A	r Speed lsb [1/100 m/s]
0x3B	r Speed msb [1/100 m/s]
0x3C	r Heading lsb [1/10000 rad → North]
0x3D	r Heading msb [1/10000 rad → North]
0x3E	r/w New data ready 1=new data, old=0

Module address	(0x10 in PicWatch)
0x22	r RC Signal no signal = 0, signal =1
0x23	r Signal source RC=0 AP=1
0x24	r LED switch OFF=0 ON=1
0x30	r RC receiver channels 1 to 8 + 2
	Value is between 0-1024
0x39	channel 5 is RC/AP switch
0x40	r/w Autopilot channels 1 to 8 + 2
	Value is between 0-1024
0x49	



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Autopilot power consumption



Table 5.2: Power consumption of the avionics subsystems

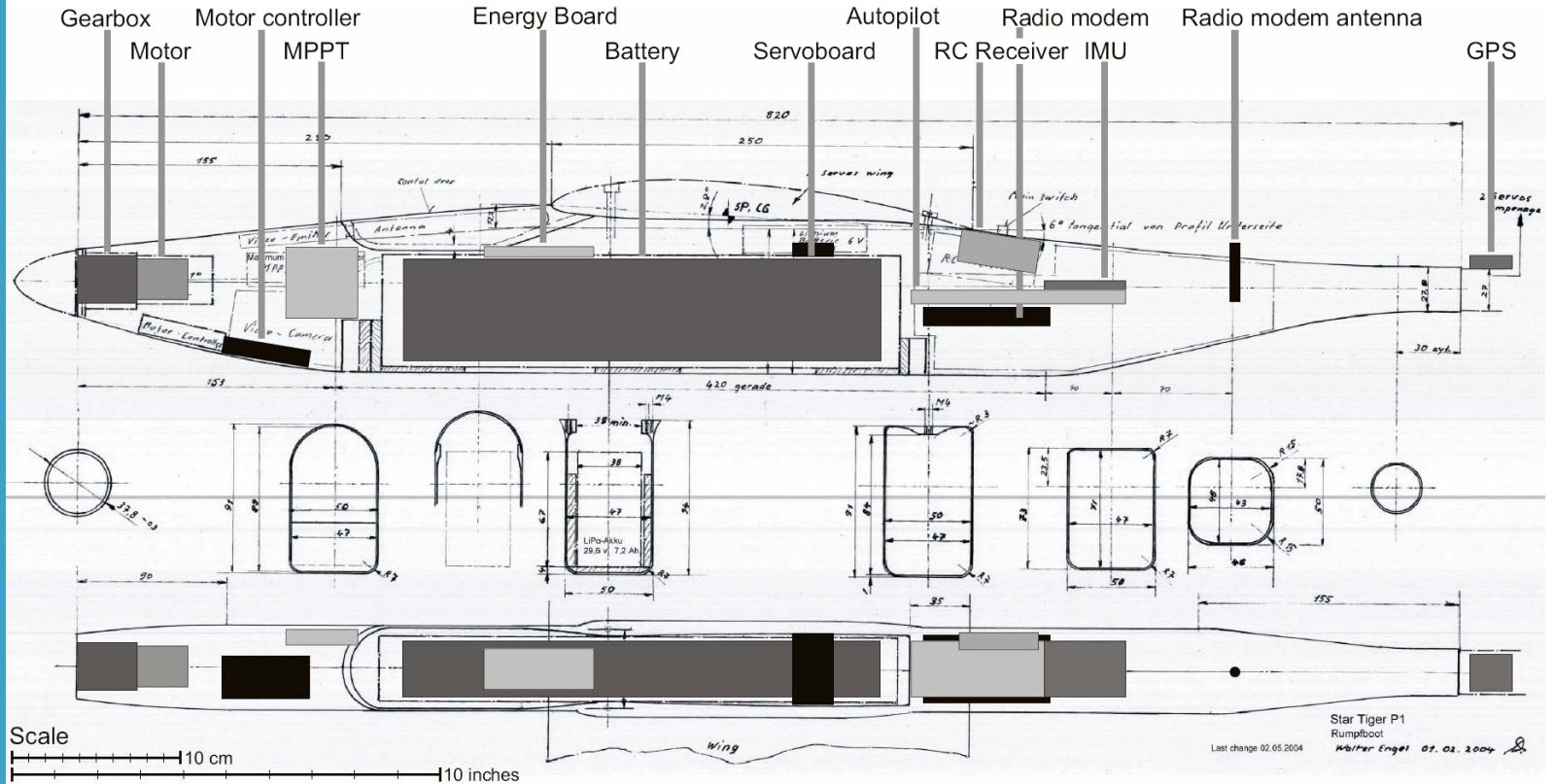
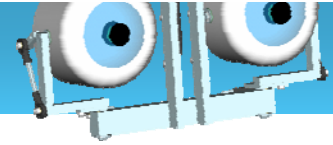
Device	Voltage [V]	Current [mA]	Power [mW]	η_{conv} from 5.6V [-]	Power @ BEC [mW]
Radio Modem (XStream)	5	80	400	89%	449
IMU (Xsens MTX)	5	70	360	89%	404
CSDX (Sensortech)	5	7	35	89%	39
Pic16F876-Autopilot	5	7	35	89%	39
Pic16F876-Energy Board	5	7	35	89%	39
MS5534 (Intersema)	3.3	1	33	92%	36
GPS (Nemerix NB1043)	3.3	20	66	92%	72
DsPic33-Autopilot	3.3	27	99	92%	108
DsPic33-Servoboard	3.3	27	99	92%	108
Pic16LF877-Autopilot	3.3	5	17	92%	18
Total			1.179		1.313



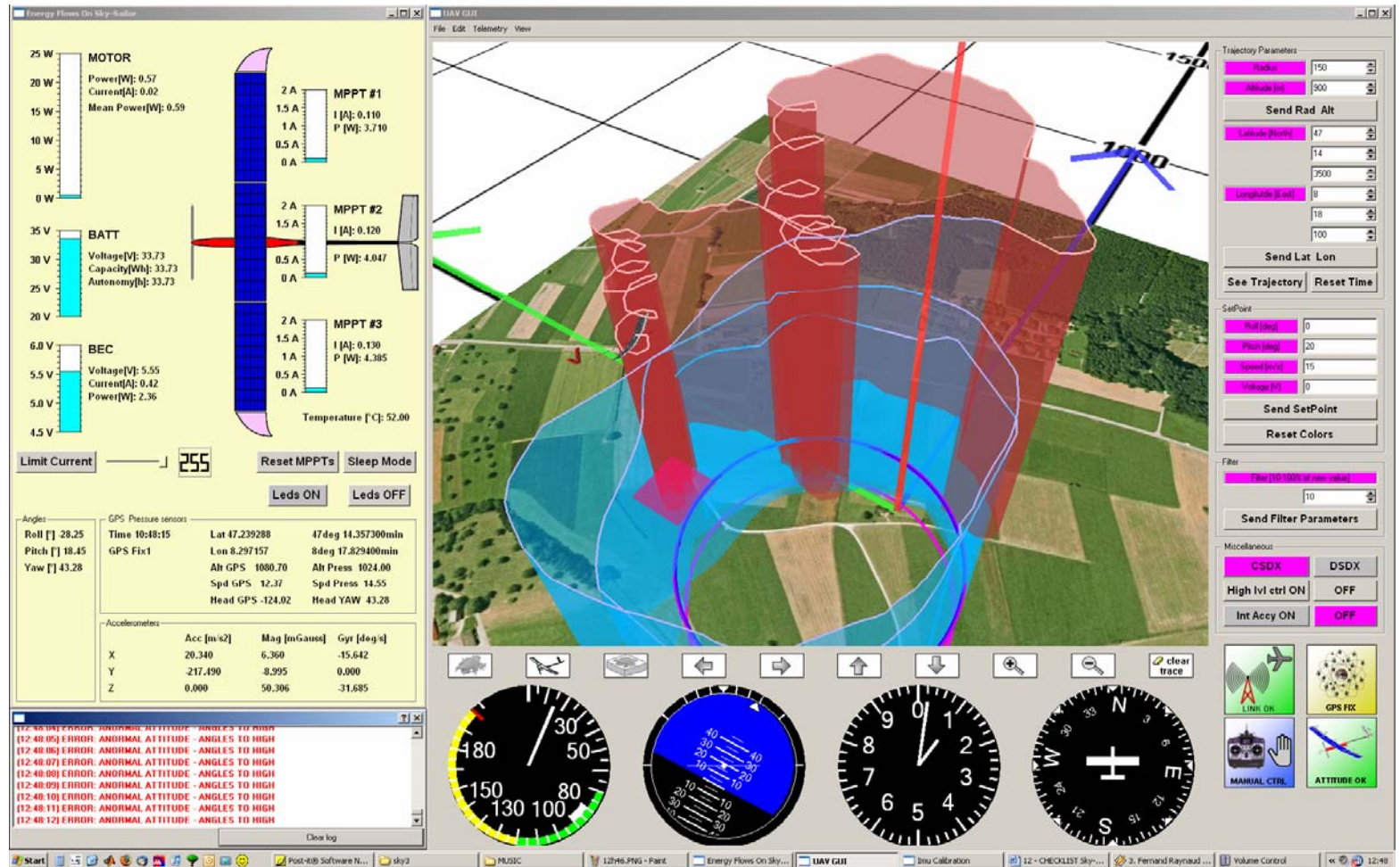
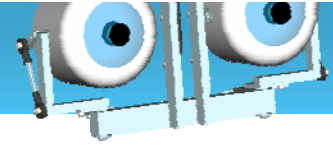
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Element placement in fuselage

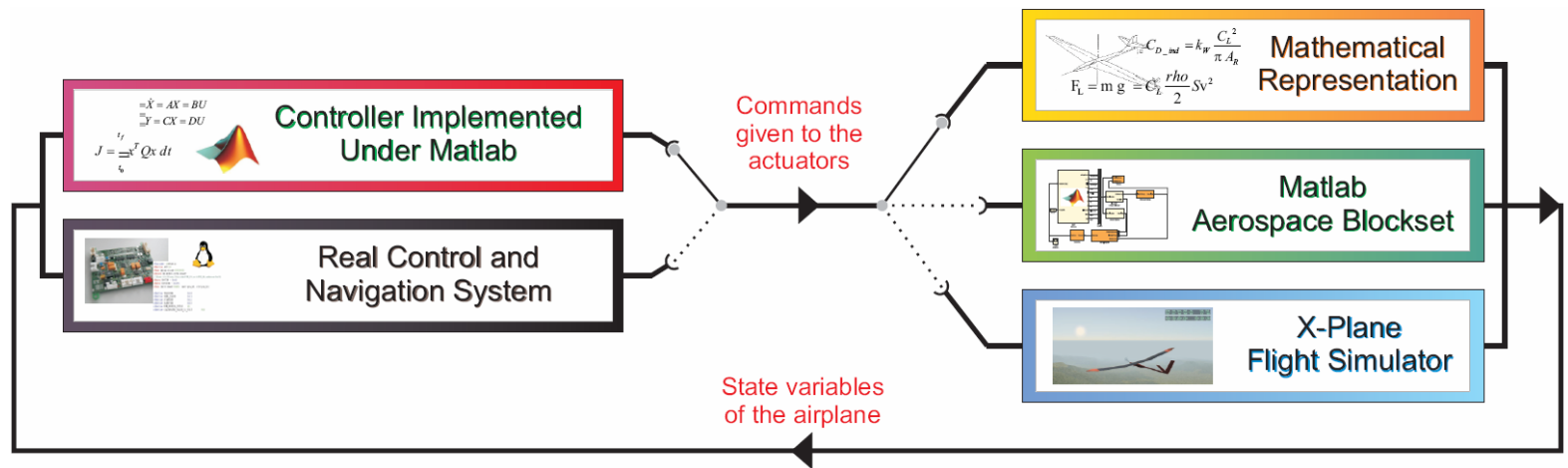
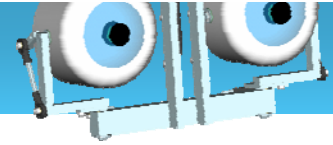


GUI (thermals)



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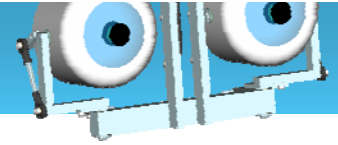
Modeling & Simulation



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Overall



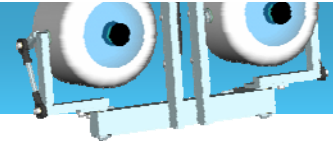
Overall



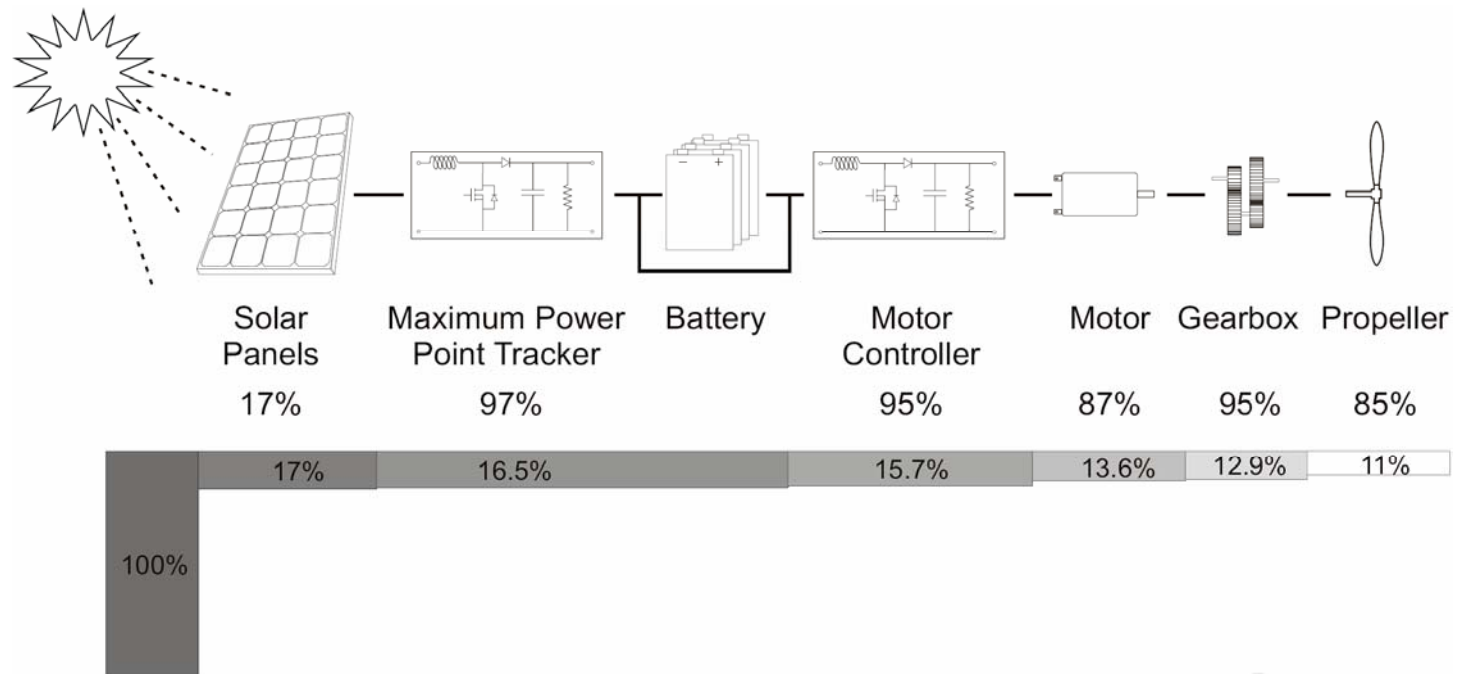
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Energy chain

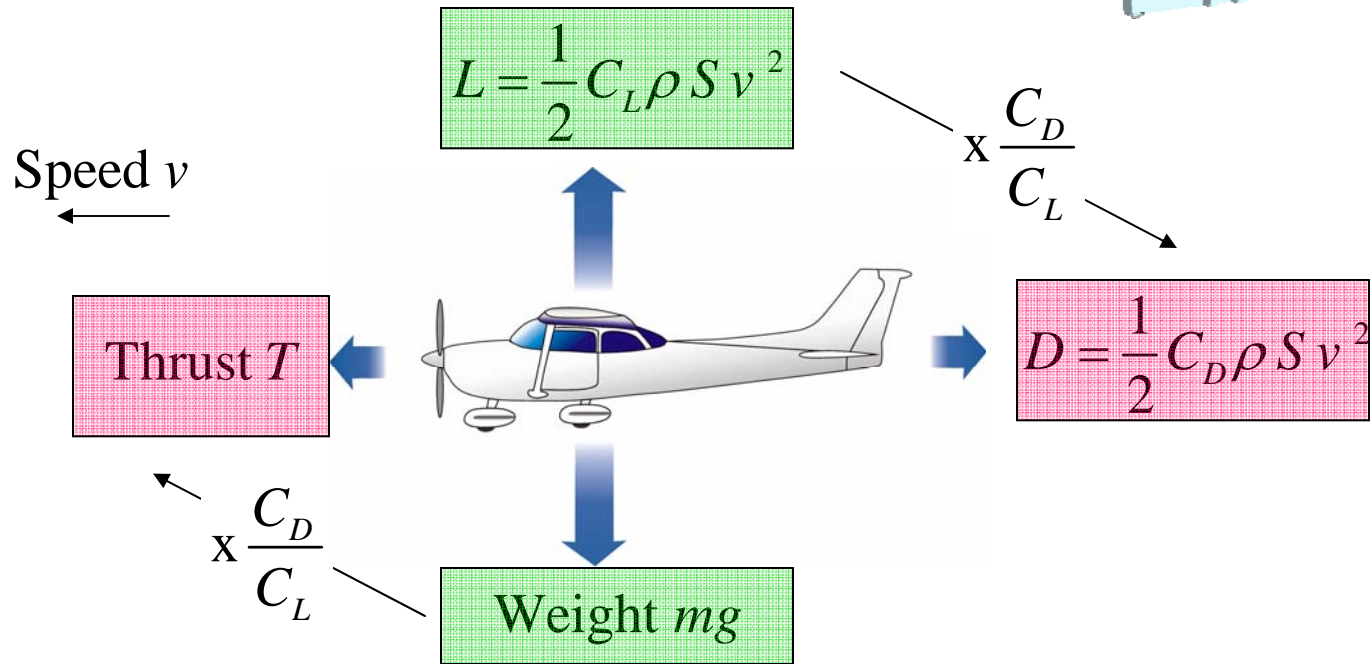
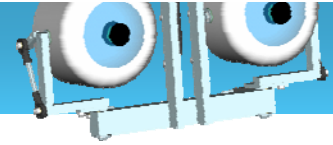


A succession of losses....



→ Important to ↗ efficiencies

Why are solar airplanes large and slow ?



1. Equilibrium of forces
2. Ratio between L and D is equal to C_L/C_D
 - the same ratio occurs between thrust and weight
 - independent of v , it only requires Sv^2 constant
3. Power for level flight is thus $P_{\text{required}} = T \cdot v = (mg \cdot C_D / C_L) \cdot v$
4. A way to reduce the power is to lower the speed v
 - in order to keep the lift (Sv^2 constant), S needs to be increased

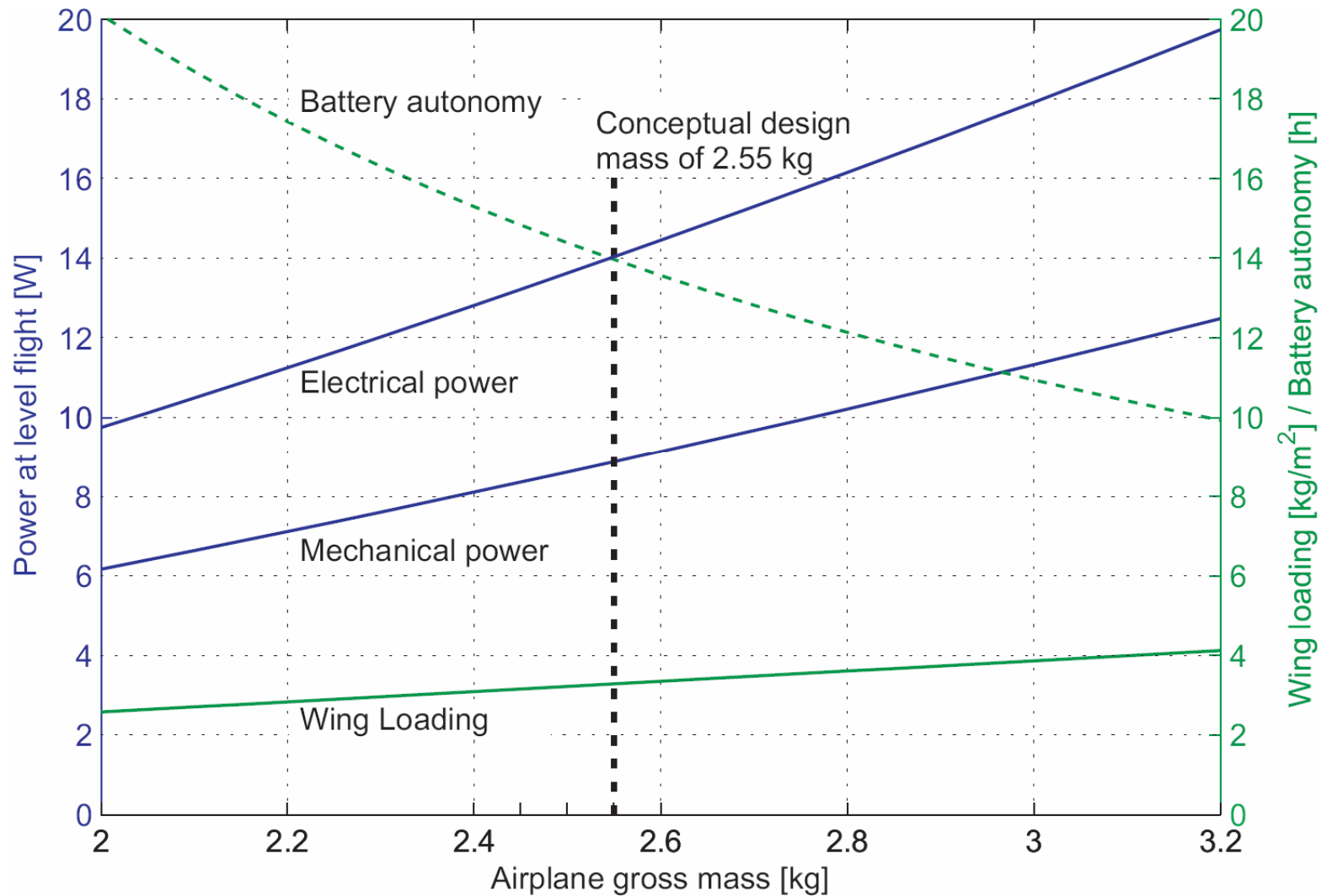


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→ Solar airplanes generally have large wings and a low speed

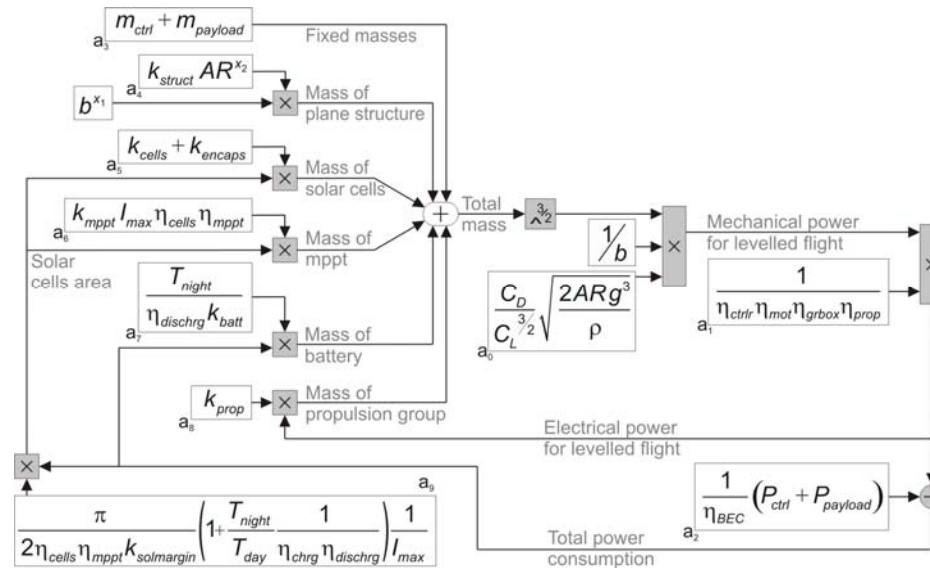
Weight – Power - Autonomy



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Methodology Resolution



$$m = m_{ctrl} + m_{payload} + m_{struct} + m_{solar} + m_{batt} + m_{mppt} + m_{prop}$$

$$m - a_0 a_1 (a_7 + a_8 + a_9 (a_5 + a_6)) \frac{1}{b} m^{\frac{3}{2}} = a_2 (a_7 + a_9 (a_5 + a_6)) + a_3 + a_4 b^{x_1}$$

The equation of the total mass is

$$m - a_{10} \frac{1}{b} m^{\frac{3}{2}} = a_{11} + a_4 b^{x_1}$$

It can be shown that it has a solution if:

$$a_{12}^2 a_{13} \leq \frac{4}{27}$$



30 Parameters



Table 1 Parameters that are constant or assumed constant

Parameter	Value	Unit	Description
C_L	0.8	-	Airfoil lift coefficient
C_{Da}	0.013	-	Airfoil drag coefficient
e	0.9	-	Oswald's efficiency factor
I_{max}	950	[W/m ²]	Maximum irradiance
k_{batt}	190.3600	[J/kg]	Energy density of battery
k_{cells}	0.32	[kg/m ²]	Mass density of solar cells
k_{encaps}	0.22	[kg/m ²]	Mass density of encapsulation
k_{mppt}	0.00047	[kg/W]	Mass to power ratio of mppt
k_{prop}	0.013	[kg/W]	Mass to power ratio of propulsion unit
k_{struct}	0.44/9.81	[kg/m ³]	Structural mass constant
m_{elec}	0.25	[kg]	Mass of navigation & control system
η_{bec}	0.7	-	Efficiency of step-down converter
η_{cells}	0.169	-	Efficiency of solar cells
η_{chrg}	0.98	-	Efficiency of battery charge
η_{ctrl}	0.95	-	Efficiency of motor controller
$\eta_{dischrg}$	0.98	-	Efficiency of battery discharge
η_{grbox}	0.95	-	Efficiency of gearbox
η_{mot}	0.85	-	Efficiency of motor
η_{mppt}	0.97	-	Efficiency of mppt
η_{prop}	0.85	-	Efficiency of propeller
P_{ctrl}	1	[W]	Power of navigation & control system
x_1	3.1	-	Structural mass area exponent
x_2	-0.25	-	Structural mass aspect ratio exponent

Table 2 Parameters determined by the mission

Parameter	Value	Unit	Description
$k_{solmargin}$	0.7	-	Irradiance margin factor
$m_{payload}$	0.25	[kg]	Payload mass
$P_{payload}$	0.5	[W]	Payload power consumption
ρ	1.1655	[kg/m ³]	Air density (500 m)
T_{day}	14.3600	[s]	Day duration

Table 3 Variables linked to the airplane shape

Parameter	Value	Unit	Description
AR	12.9	-	Aspect ratio
b	3.2	[m]	Wingspan
m	2.6	[kg]	Total mass



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Sky-Sailor weight distributions

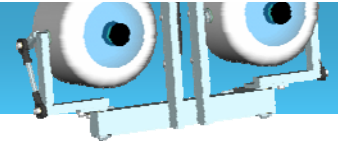


Part	Dimensions [mm]	Mass [g]
Motor Controller	52 x 25 x 10	20
Brushless motor (Strecker)	∅30 x 25	55.3
Gearbox	∅33 x 29	29.7
Solariane Propeller & mounting piece	600	34.05
Lipo-Akku	283 x 60 x 33	1056.00
MPPT + Shielding	42 x 42.5 x 9	25.86
Energy board (Incl. BEC & Shield)	65 x 24 x 6	17.70
Autopilot sensor board	127 x 33 x 8	8.37
IMU	48 x 33 x 13.5	15.00
GPS & patch antenna	25 x 22 x 8	10.96
Servoboard	42 x 24 x 8	6.51
RC Receiver	47 x 19 x 10	9.80
RC Receiver Antenna	1000	1.30
Radio Modem & Antenna	75 x 40 x 11	26.48
On/Off Switch	23 x 14 x 13	4.85
Wing part middle (complete)	980 x 250 x 25	302
Wing part left (complete)	1130 x 300 x 25	266
Wing part right (complete)	1130 x 300 x 25	270
3 Wing Screw M4		0.95
Fuselage with tail boom	1720 x 94 x 54	168.85
2 V-Tails	41.5 x 15.5 x 1.2	54
Cables		To be def.
Total take-off mass(21.06.2008)	3240 x 1818 x 295	2444.00



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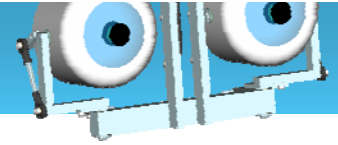
Applications



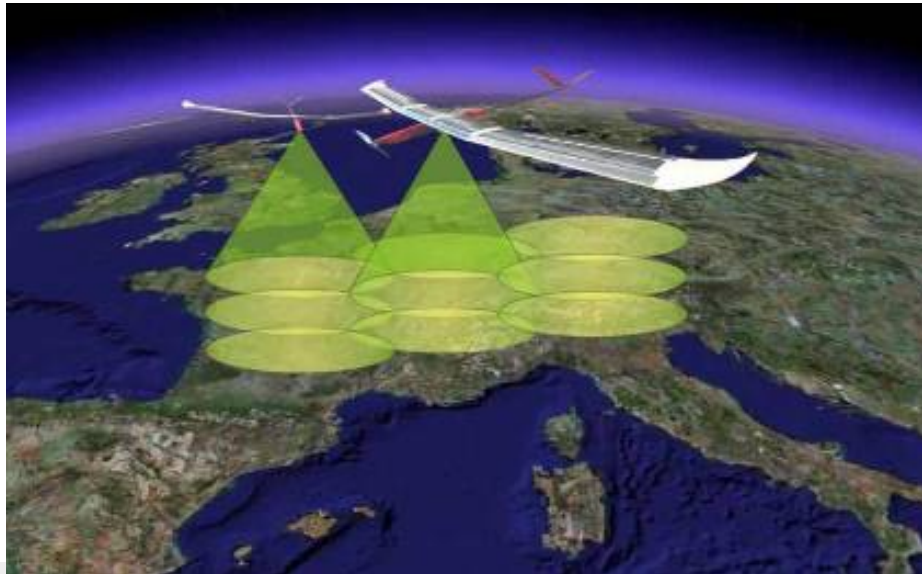
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Potential Applications



- high altitude communication platform
- law enforcement
- border surveillance
- forest fire fighting
- power line inspection
- ...



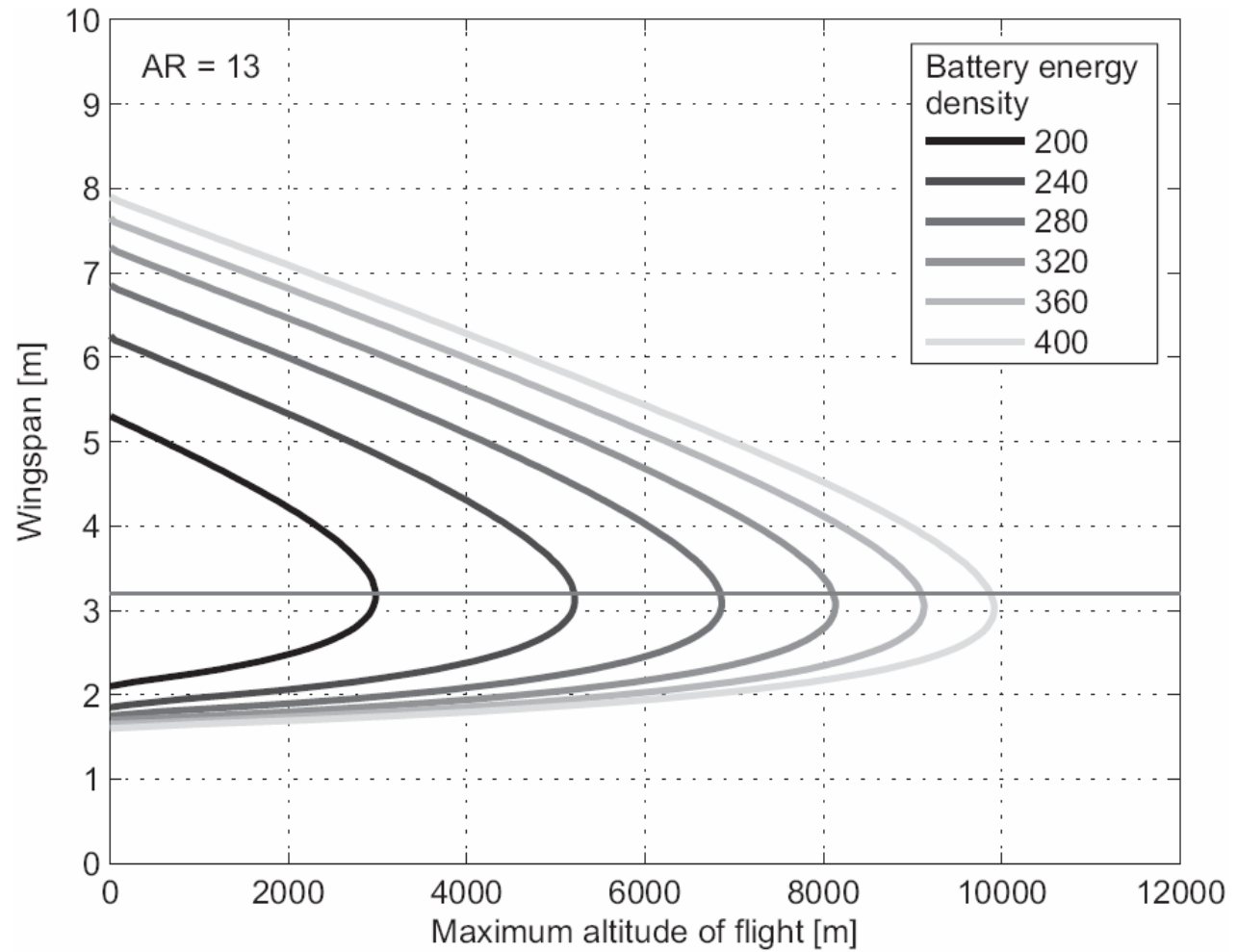
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Sky-Sailor



What is the influence of battery technology on the maximal flying altitude ?



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MAV

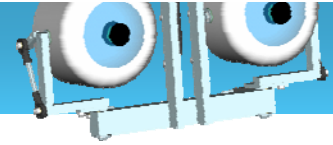
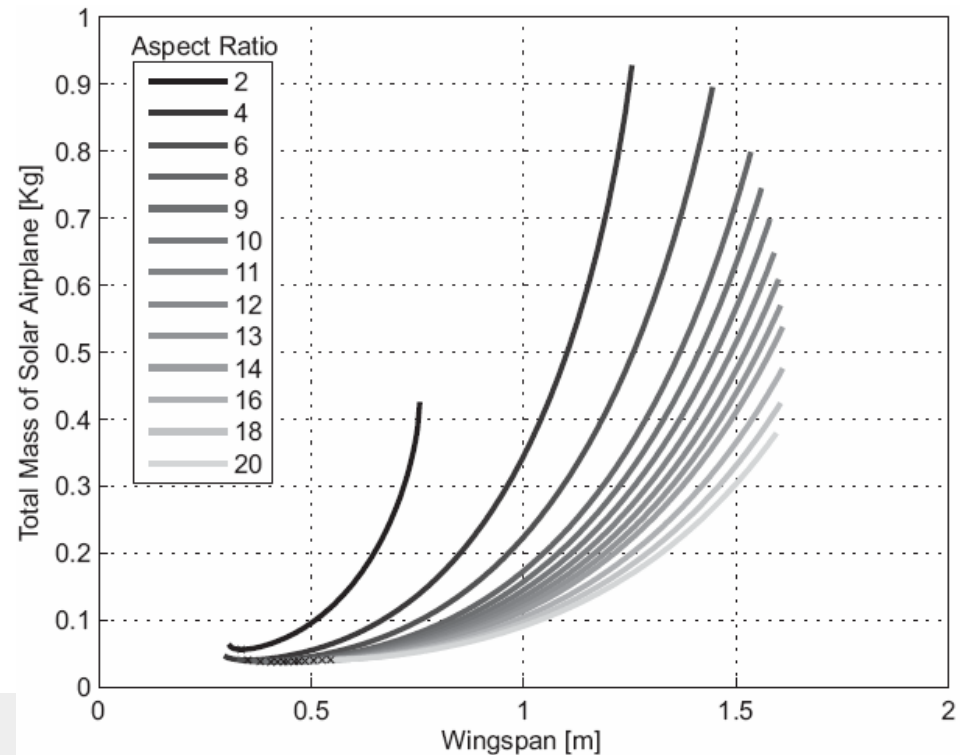


Table 6.1: Parameters changes at the MAV size

Parameter	Value	Unit	Description
C_L	0.5	-	Airfoil lift coefficient
$C_{D_{aft}}$	0.05	-	Airfoil drag coefficient
e	0.6	-	Oswald's efficiency factor
k_{af}	5.58/9.81	$[kg/m^3]$	Structural mass constant
m_{av}	0.005	$[kg]$	Mass of autopilot system
η_{grb}	0.81	-	Efficiency of gearbox
η_{mot}	0.62	-	Efficiency of motor
η_{plr}	0.80	-	Efficiency of propeller
P_{av}	0.1	$[W]$	Power of autopilot system
x_1	3.18	-	Airframe mass area exponent
x_2	-0.88	-	Airframe mass aspect ratio exponent
m_{pld}	0.01	$[kg]$	Payload mass
P_{pld}	0.00	$[W]$	Payload power consumption



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MAV

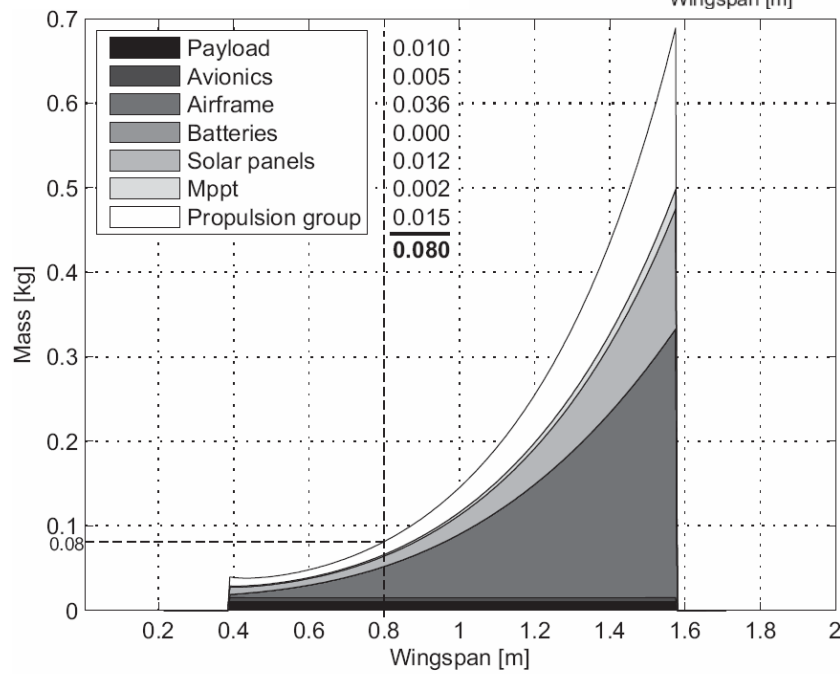
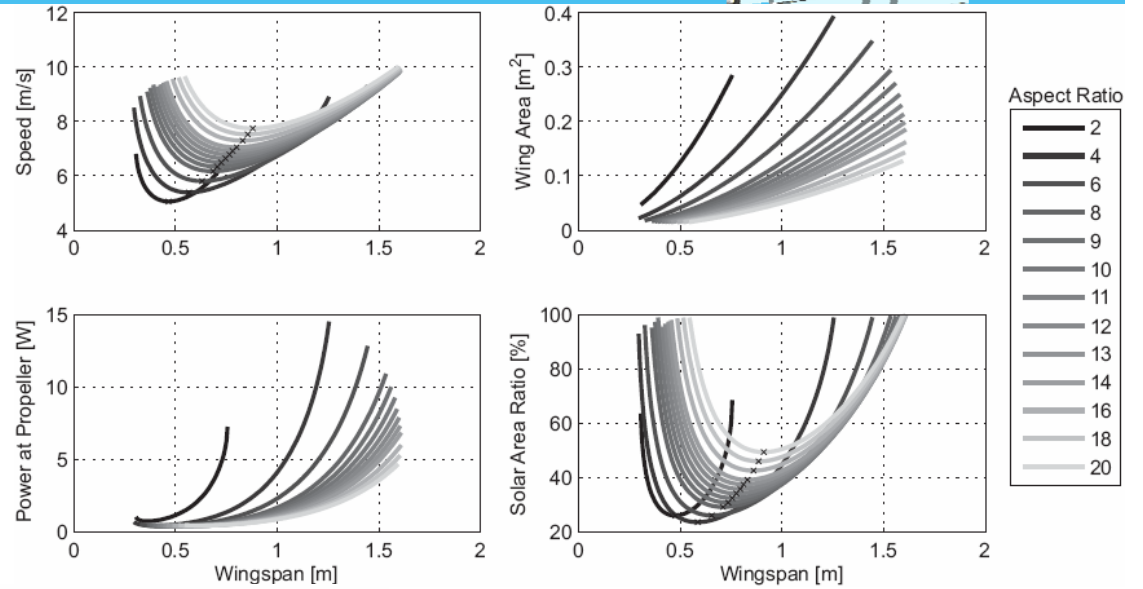


Figure 6.4: Mass distribution for $AR = 10$



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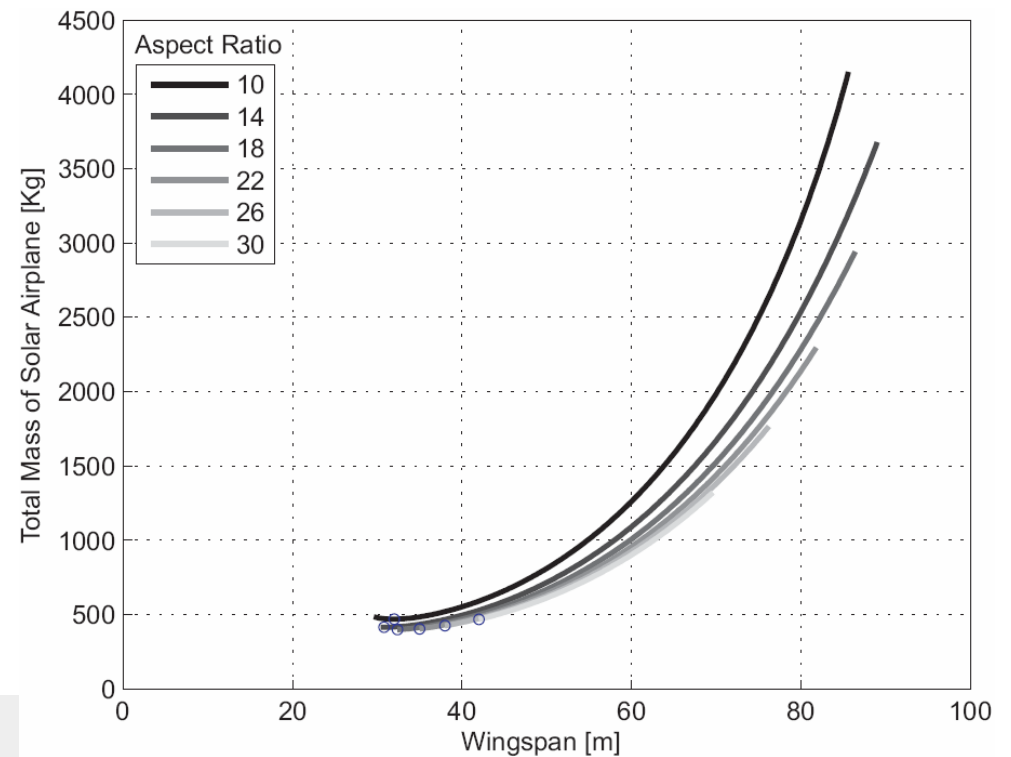
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Manned



Table 6.2: Parameters changes at the manned airplane size

Parameter	Value	Unit	Description
C_L	1	-	Airfoil lift coefficient
k_{prop}	0.00121	$[kg/W]$	Mass to power ratio of prop. group
k_{af}	0.44/9.81/15	$[kg/m^3]$	Structural mass constant
m_{av}	20	$[kg]$	Mass of autopilot system
η_{sc}	0.19	-	Efficiency of solar cells
η_{ctrl}	0.98	-	Efficiency of motor controller
η_{mot}	0.88	-	Efficiency of motor
η_{plr}	0.87	-	Efficiency of propeller
P_{av}	100	$[W]$	Power of autopilot system
m_{pld}	120	$[kg]$	Payload mass
P_{pld}	0	$[W]$	Payload power consumption



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Manned

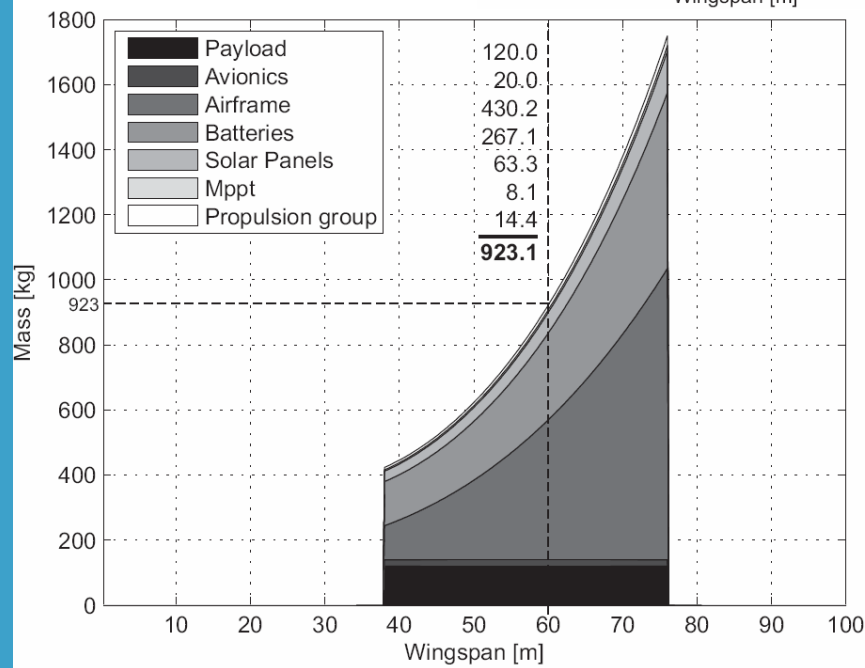
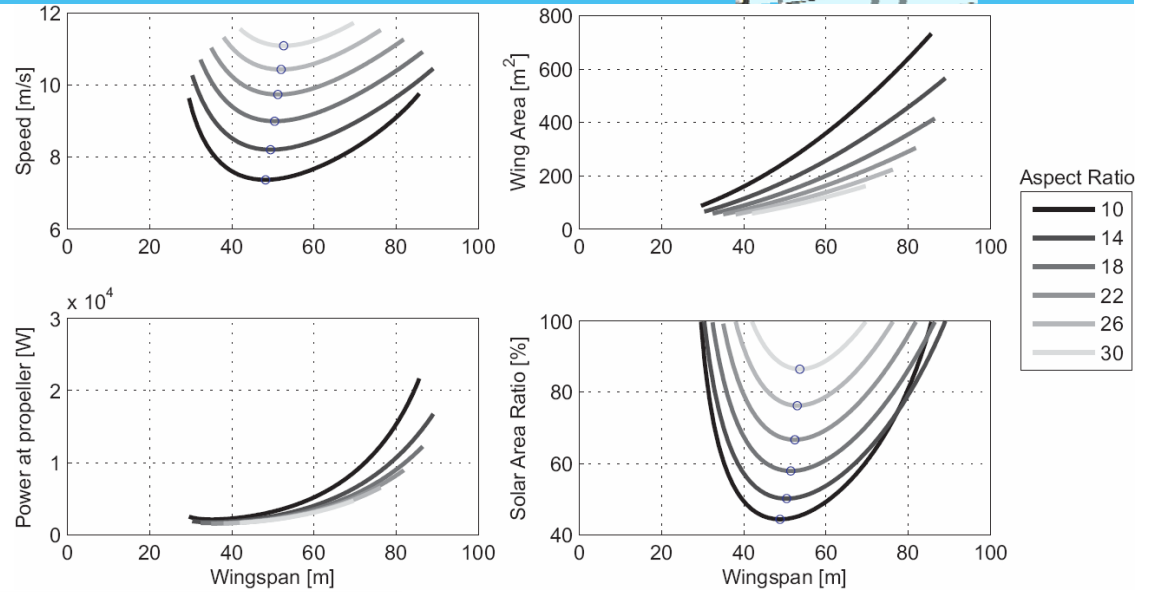


Figure 6.7: Mass distribution for $AR = 10$



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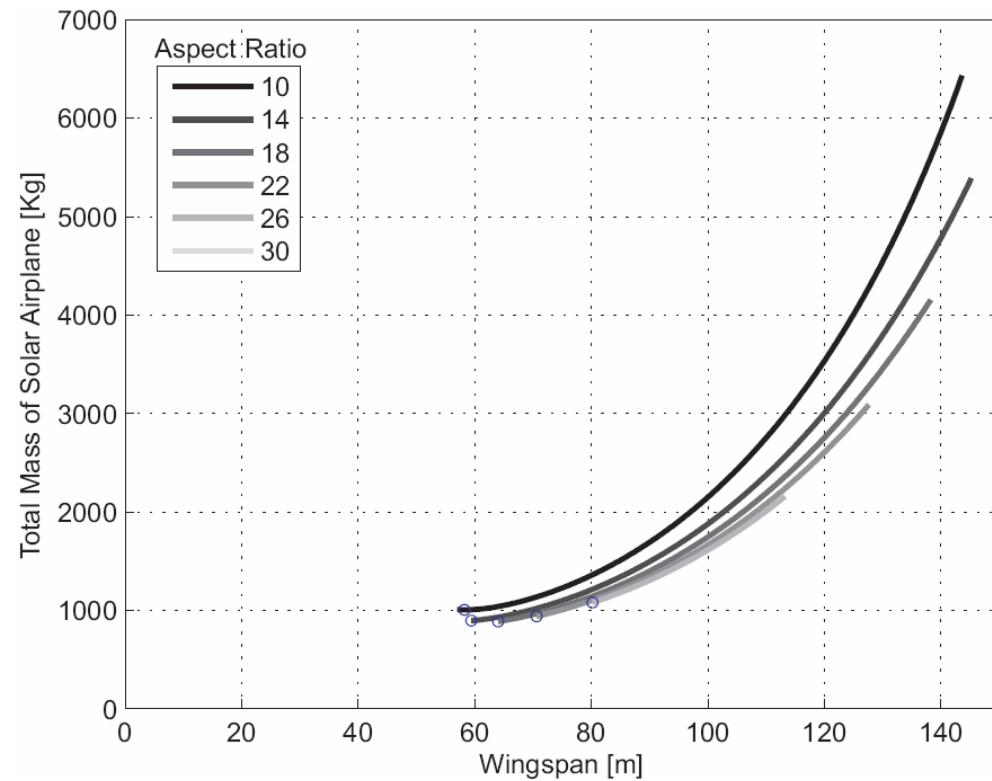
HALE Platform



Payload: 300 Kg

Altitude: 21'000 m

Mission time: 3 months in summer



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HALE Platform

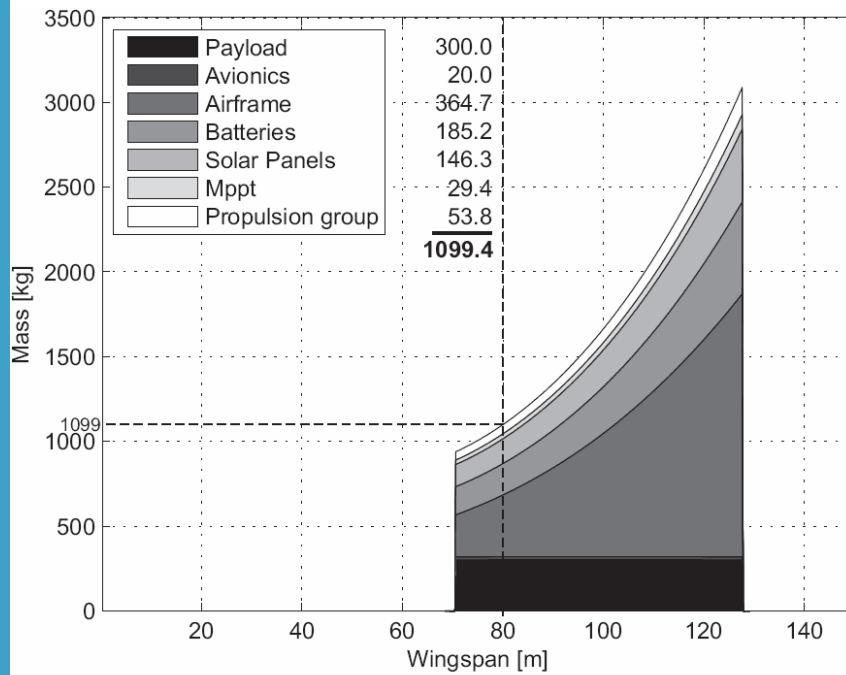
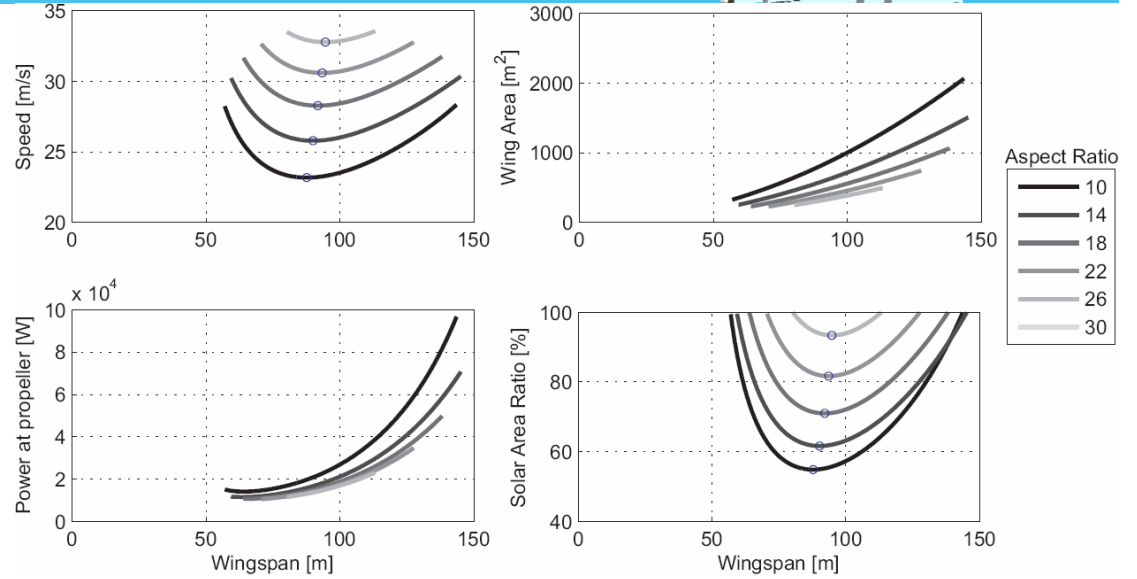


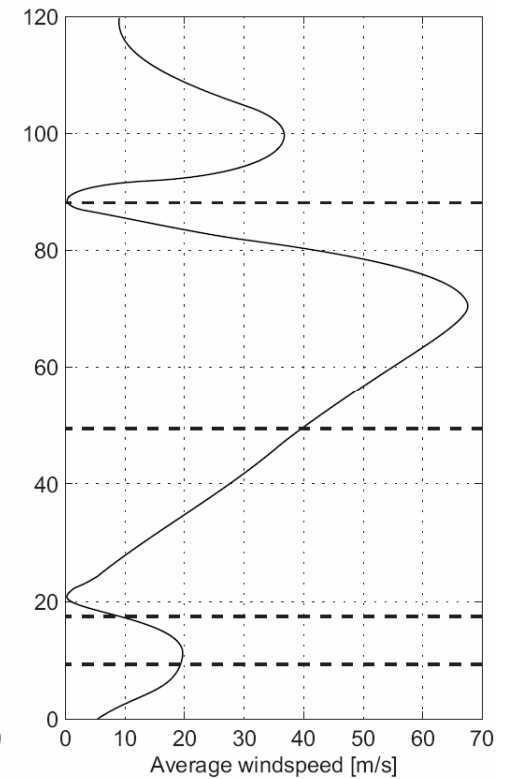
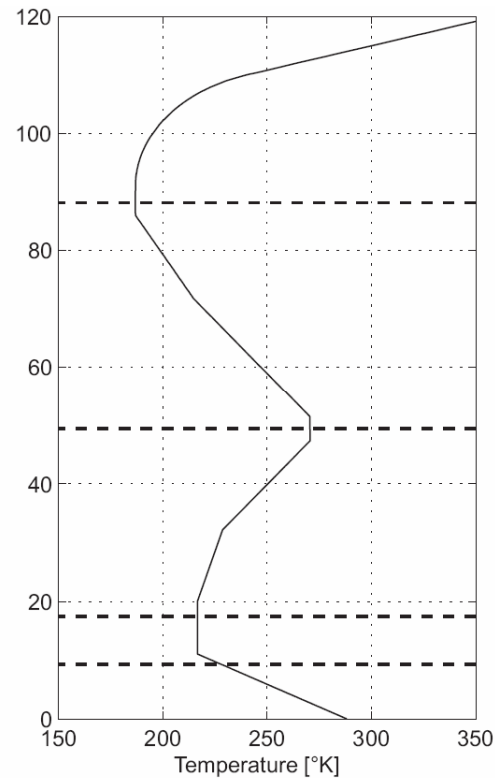
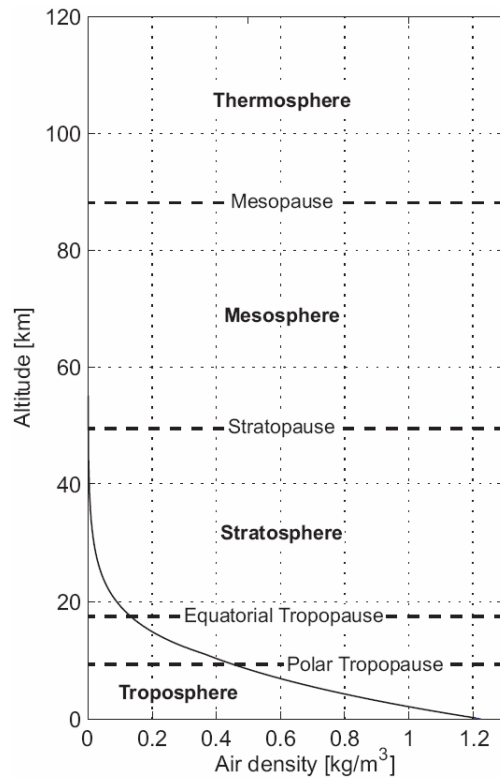
Figure 6.12: Mass distribution for $AR = 22$



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HALE Platform



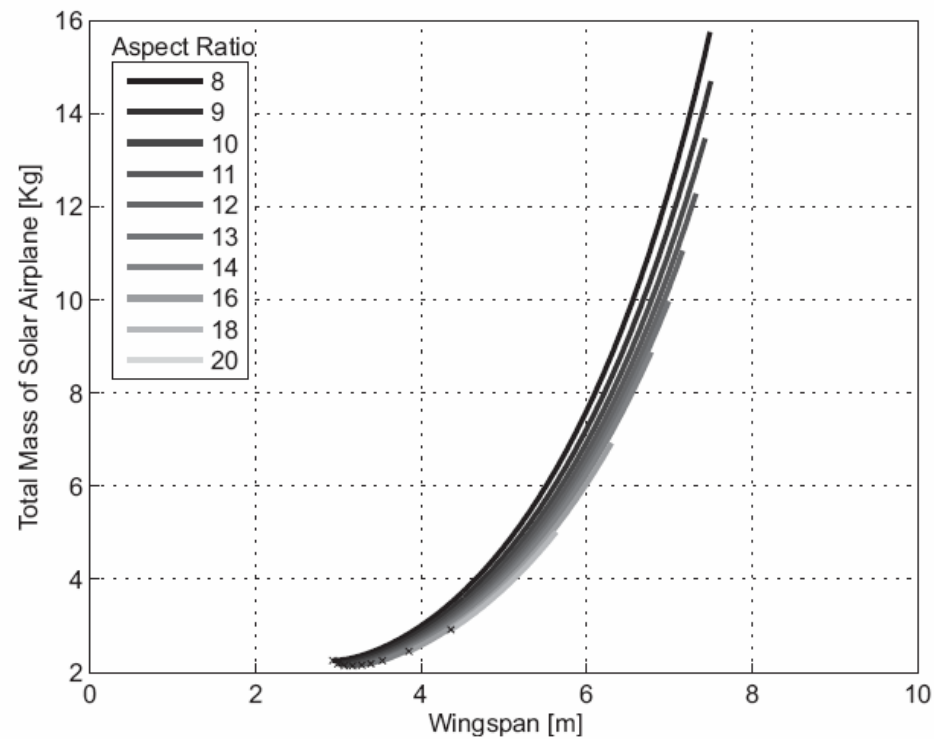
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Mars design



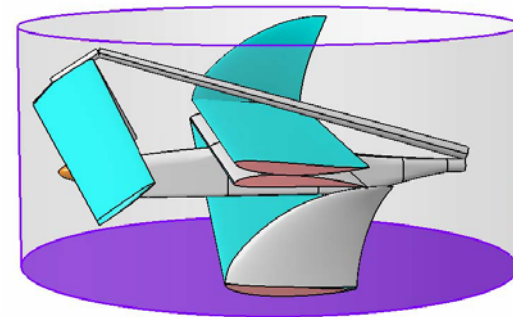
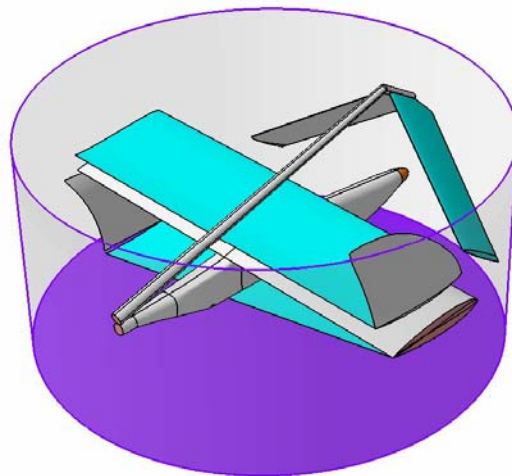
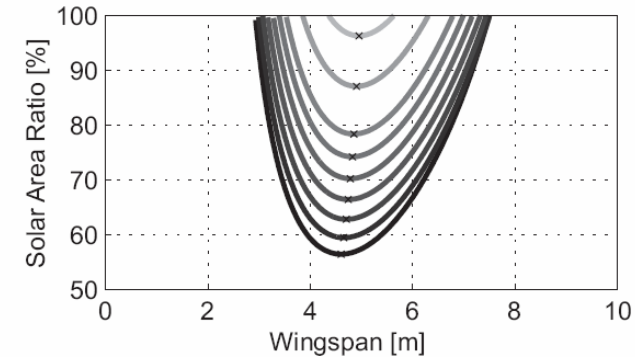
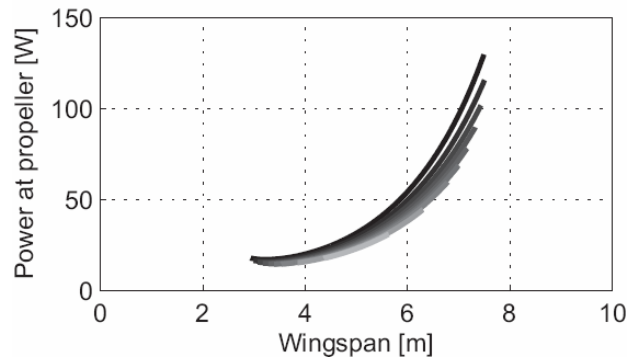
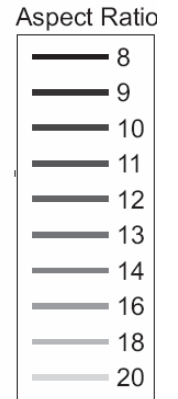
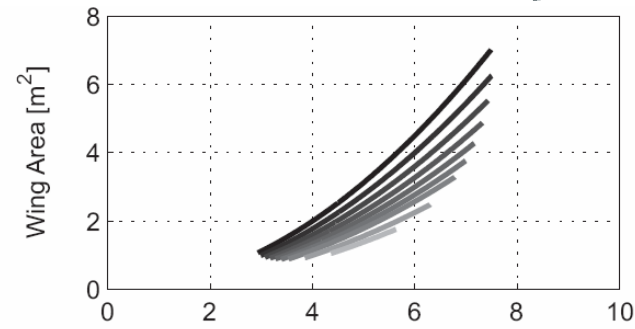
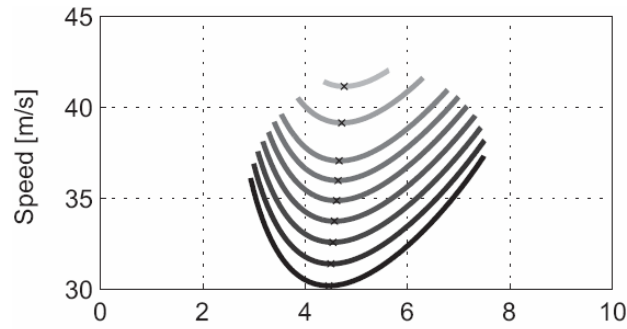
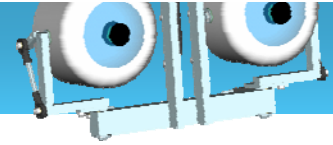
Parameter	Value	Unit	Description
I_{max}	589	$[W/m^2]$	Maximum Irradiance
k_{bat}	1000·3600	$[J/kg]$	Energy density of energy storage
k_{af}	0.44/9.81/2	$[kg/m^3]$	Structural mass constant
m_{av}	0.15	$[kg]$	Mass of autopilot system
m_{pld}	0.5	$[kg]$	Payload mass
η_{wthr}	1	-	Irradiance margin factor
P_{pld}	0.5	$[W]$	Payload power consumption
ρ	0.015	$[kg/m^3]$	Air density (500 m)



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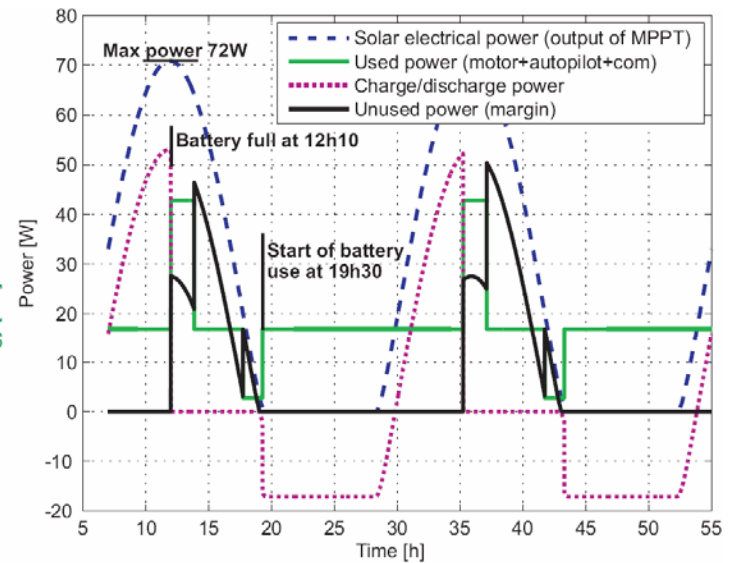
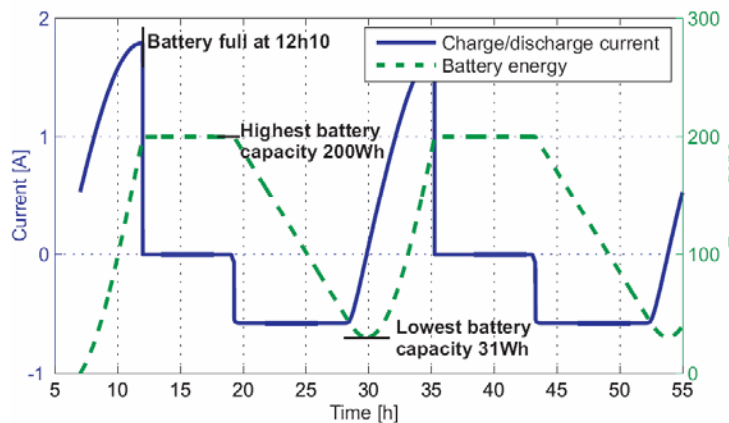
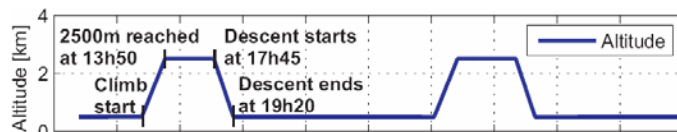
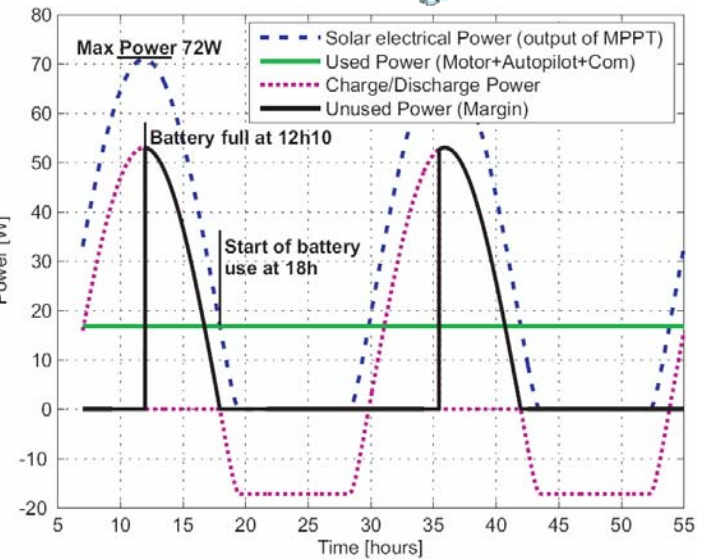
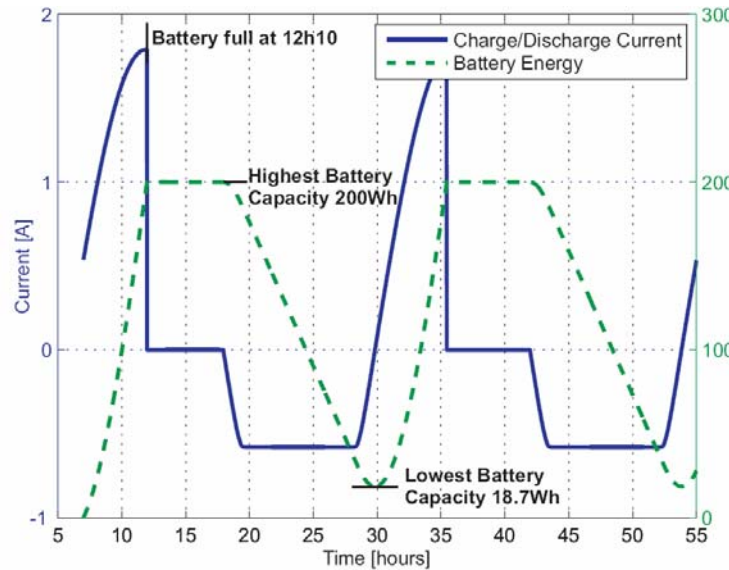
Mars design



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Storing Potential Energy

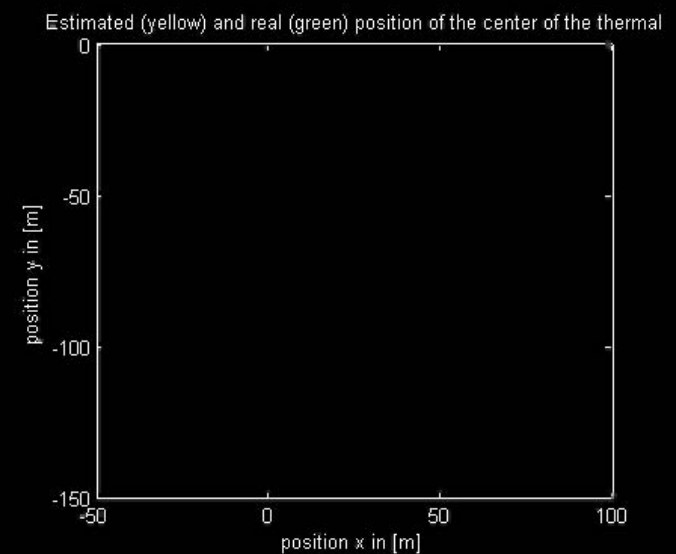
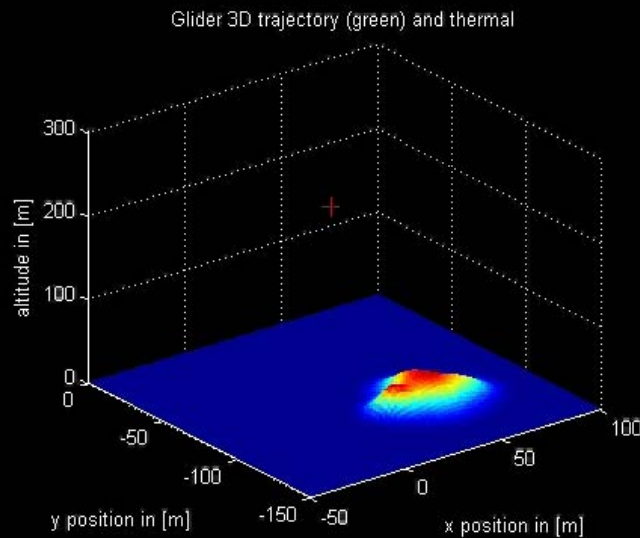
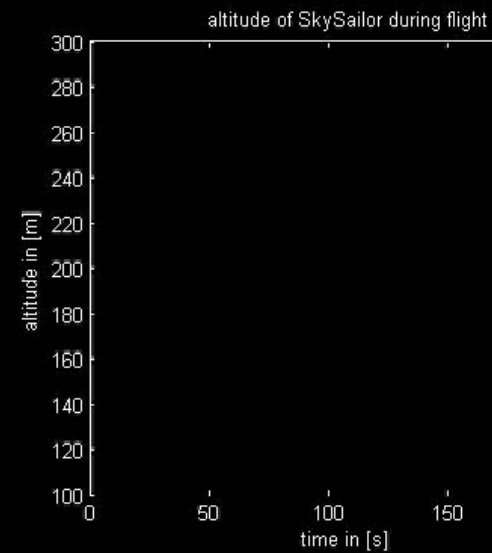
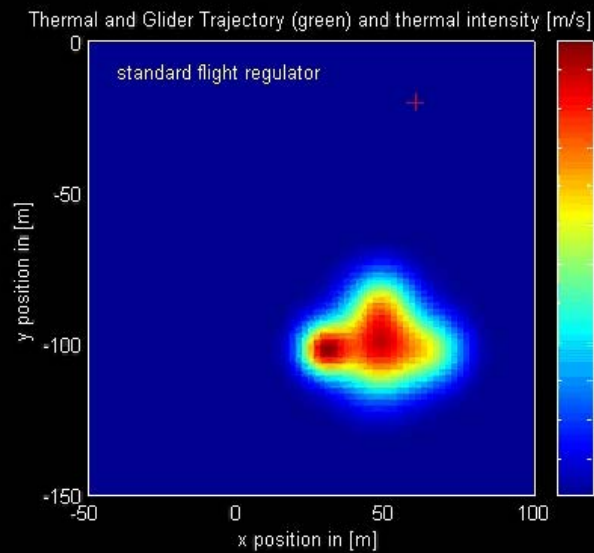


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Figure 6.13: Continuous flight simulation on the 21st of June

Using Thermals



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Link to videos:

<http://www.sky-sailor.ethz.ch/videos.htm>

Sun-Surfer



Objective:

- reduce the scale and cost
- develop low-cost solar MAVs with payload capacity of ~40 gr

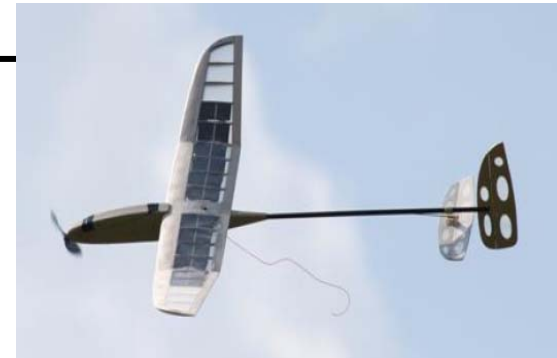
Sun-Surfer I

Wingspan: 0.77 meters

Weight: 115 g

P level flight: 1 W

P solar : 3 W



Sun-Surfer II

Wingspan: 0.78 meters

Weight: 190 g

P level flight: 2.4 W

P solar : 8 W



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Design Phases



	PHASE I CONCEPTUAL DESIGN	PHASE II PRELIMINARY DESIGN	PHASE III DETAIL DESIGN		
KNOWN	<ul style="list-style-type: none"> • BASIC MISSION REQMTS. • RANGE • ALTITUDE • SPEED • BASIC MATERIAL PROPERTIES σ/ρ E/ρ $\$/LB$	<ul style="list-style-type: none"> • AEROELASTIC REQMTS. • FATIGUE REQUIREMENTS • FLUTTER REQUIREMENTS • OVERALL STRENGTH REQMTS. 	<ul style="list-style-type: none"> • LOCAL STRENGTH REQUIREMENTS • PRODUCIBILITY • FUNCTIONAL REQMTS. 		
RESULTS	<table border="1"> <tr> <td> GEOMETRY <ul style="list-style-type: none"> • AIRFOIL TYPE • AR • t/c • λ • Δ </td> <td> DESIGN OBJECTIVES <ul style="list-style-type: none"> • DRAG LEVEL • WEIGHT GOALS • COST GOALS </td> </tr> </table>	GEOMETRY <ul style="list-style-type: none"> • AIRFOIL TYPE • AR • t/c • λ • Δ 	DESIGN OBJECTIVES <ul style="list-style-type: none"> • DRAG LEVEL • WEIGHT GOALS • COST GOALS 	<ul style="list-style-type: none"> • BASIC INTERNAL ARRGMT. • COMPLETE EXTERNAL CONFIG. • CAMBER, TWIST DISTRIBUTIONS • LOCAL FLOW PROBLEMS SOLVED • MAJOR LOADS, STRESSES, DEFLECTIONS 	<ul style="list-style-type: none"> • DETAIL DESIGN <ul style="list-style-type: none"> • MECHANISMS • JOINTS, FITTING, & ATTACHMENTS • DESIGN REFINEMENTS AS RESULTS OF TEST & OPER.
GEOMETRY <ul style="list-style-type: none"> • AIRFOIL TYPE • AR • t/c • λ • Δ 	DESIGN OBJECTIVES <ul style="list-style-type: none"> • DRAG LEVEL • WEIGHT GOALS • COST GOALS 				



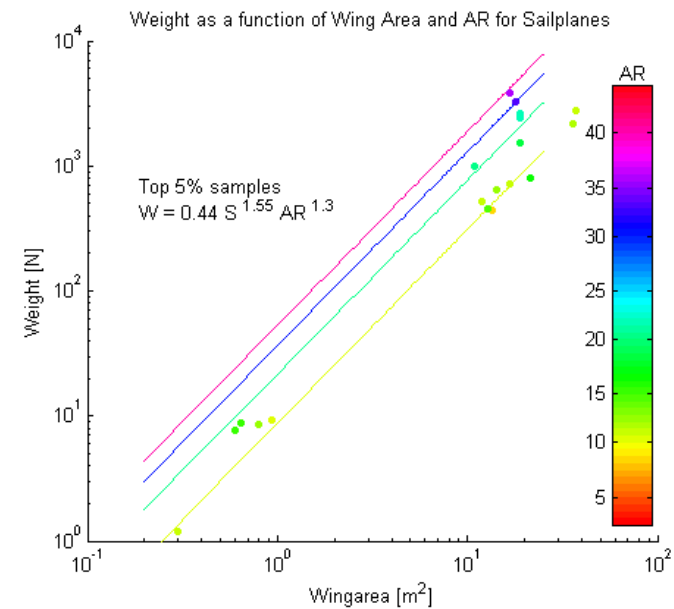
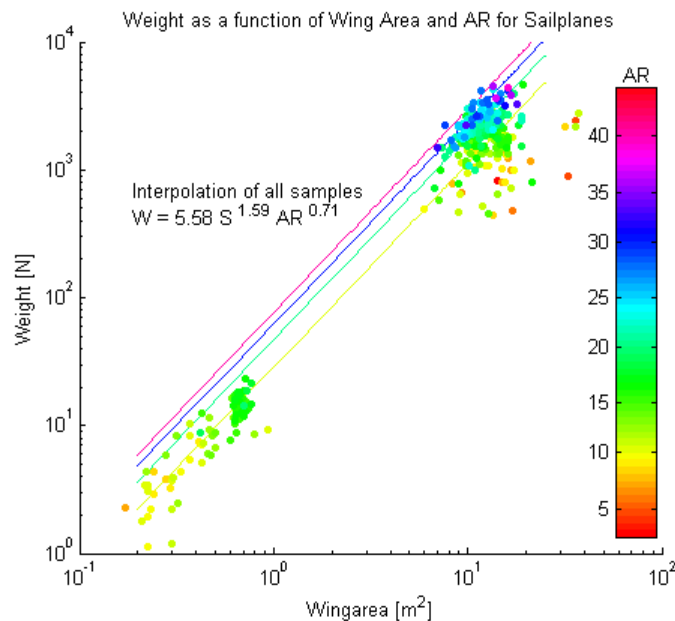
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Airframe model



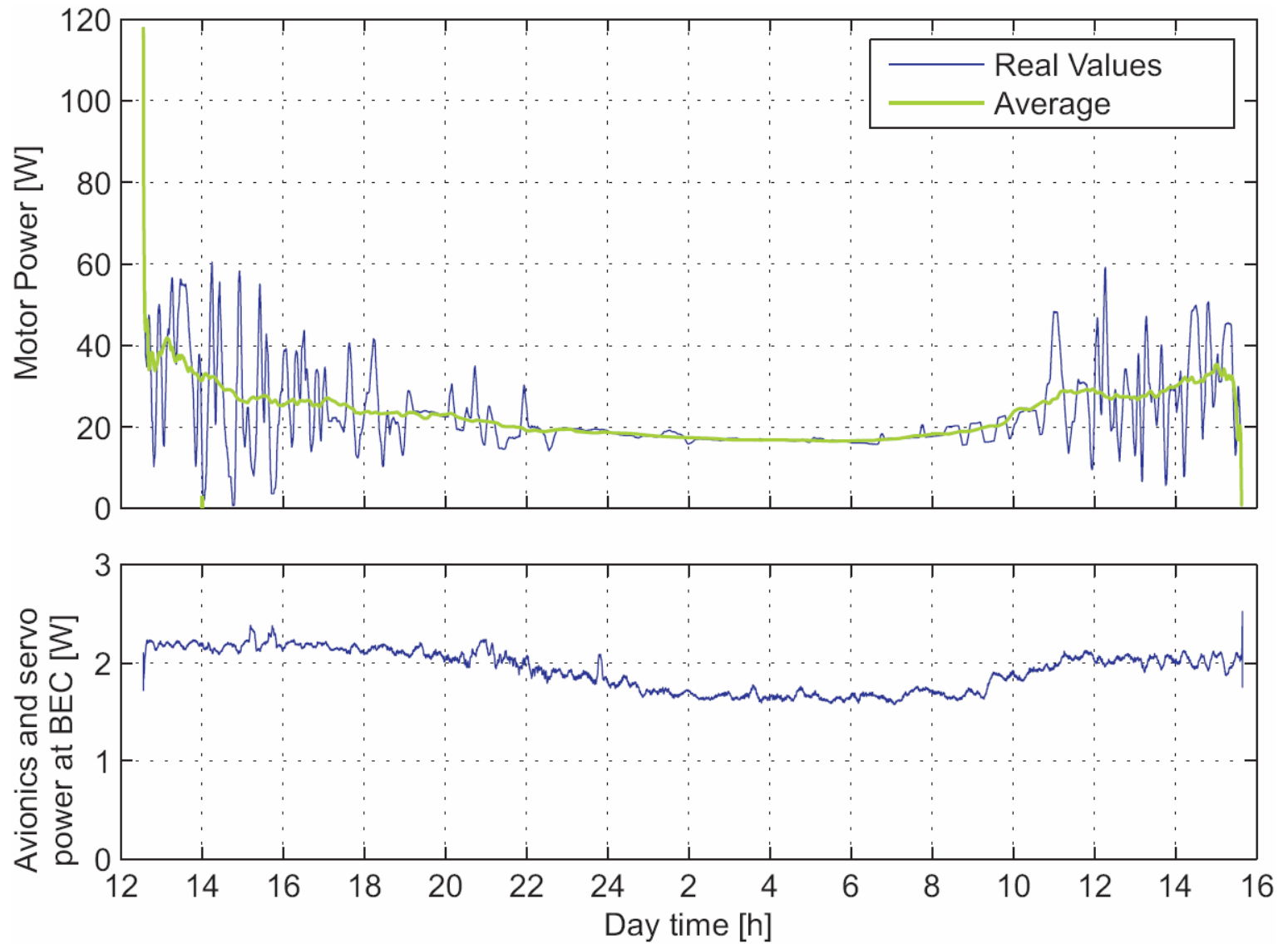
Samples	$W_{af} = f(S, AR)$	$W_{af} = f(b, AR)$	$W_{af}/S = f(W_{af}, AR)$
415	$5.58 S^{1.59} AR^{0.71}$	$5.58 b^{3.18} AR^{-0.88}$	$2.94 W_{af}^{0.37} AR^{0.45}$
260	$2.31 S^{1.58} AR^{0.94}$	$2.31 b^{3.16} AR^{-0.64}$	$1.70 W_{af}^{0.37} AR^{0.59}$
143	$1.15 S^{1.57} AR^{1.13}$	$1.15 b^{3.14} AR^{-0.44}$	$1.09 W_{af}^{0.36} AR^{0.72}$
73	$0.78 S^{1.55} AR^{1.21}$	$0.78 b^{3.10} AR^{-0.34}$	$0.85 W_{af}^{0.35} AR^{0.78}$
40	$0.56 S^{1.55} AR^{1.27}$	$0.56 b^{3.10} AR^{-0.28}$	$0.69 W_{af}^{0.35} AR^{0.82}$
19	$0.44 S^{1.55} AR^{1.30}$	$0.44 b^{3.10} AR^{-0.25}$	$0.59 W_{af}^{0.35} AR^{0.84}$



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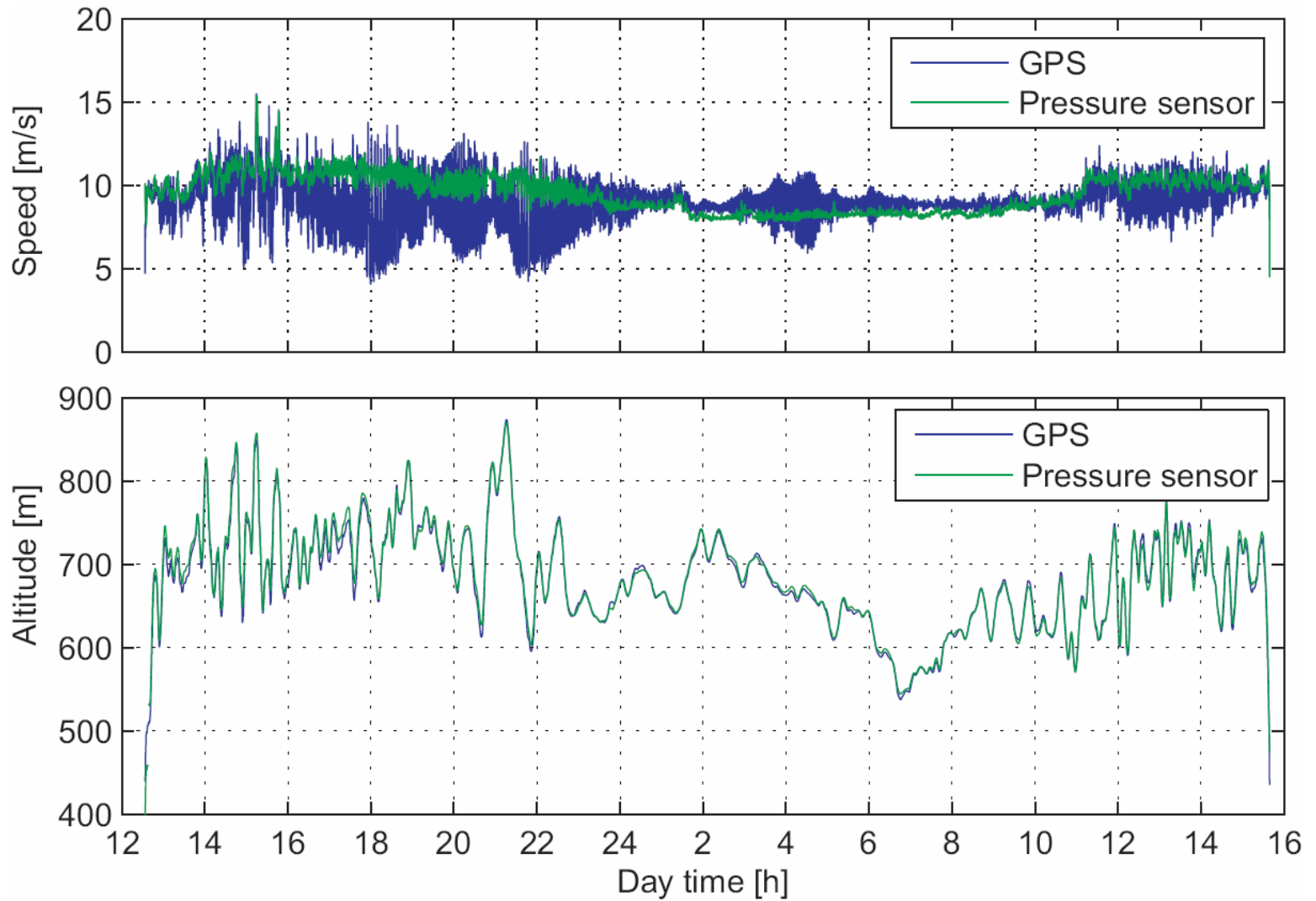
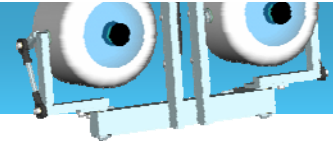
27 hours flight



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27 hours flight



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